

System Analysis of Pb-Bi Cooled Fast Reactor PEACER

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Nuclear Integrated Design Engineering Analysis

PEACER Design Focus

Proliferation-Resistance

Tech. & institutional barriers

Environment-Friendliness

Transmutation

Accident-Tolerance

Pb-Bi coolant

Continuable-Energy

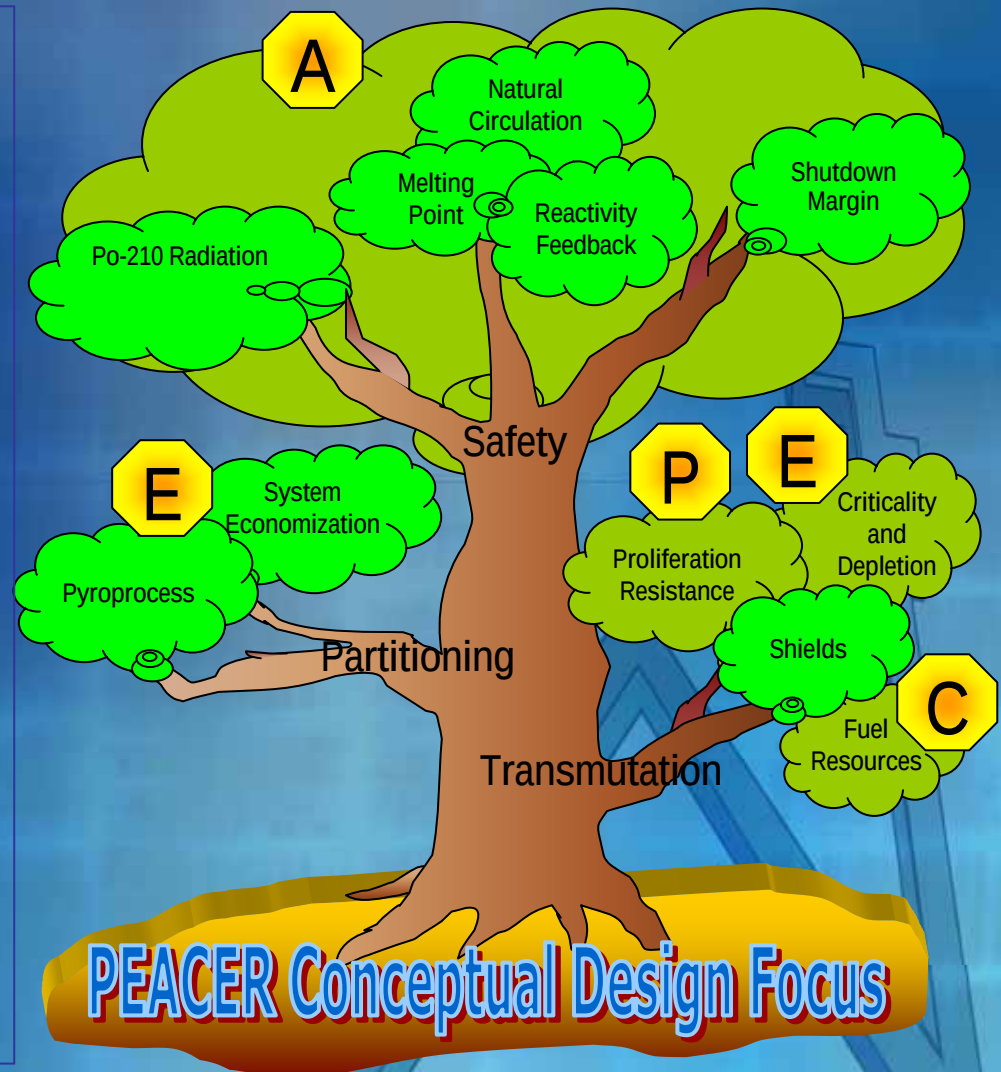
U & Th fuel

Economical

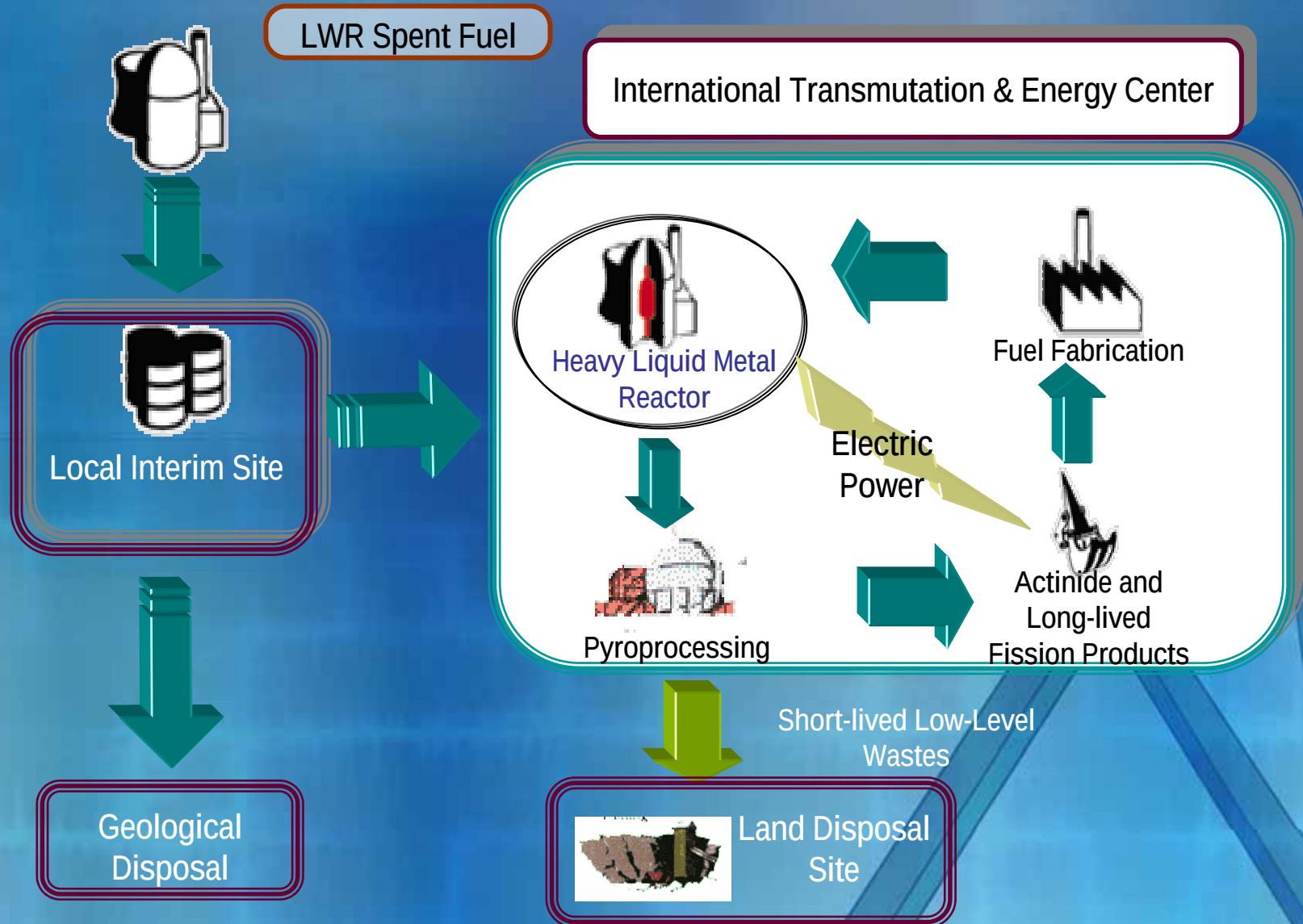
Cheap pyroprocessing

Reactor

Critical



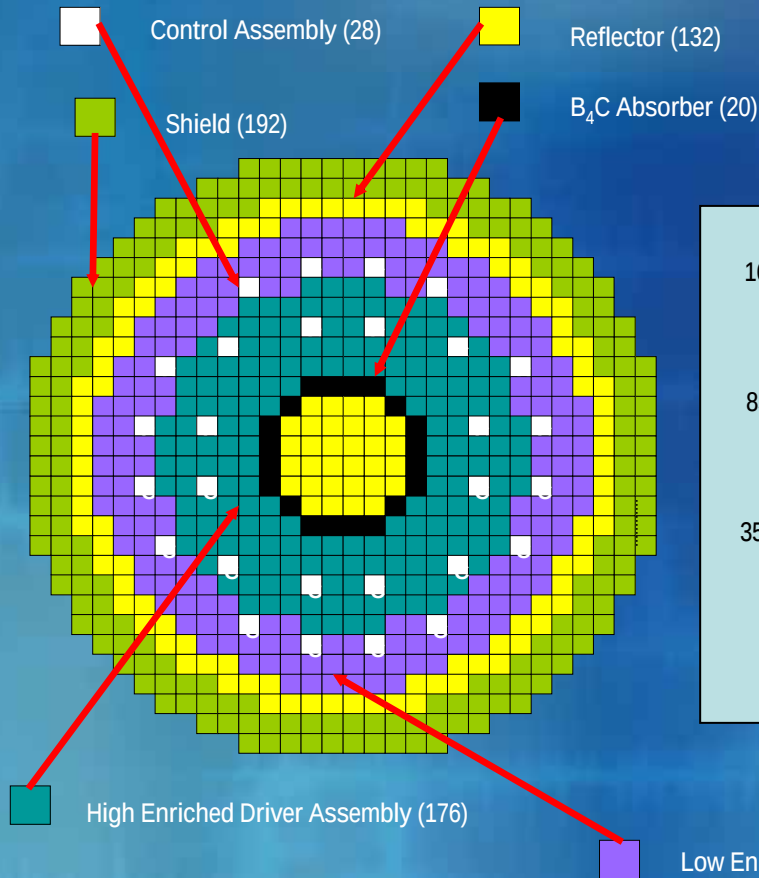
PEACER for Transmutation & Energy



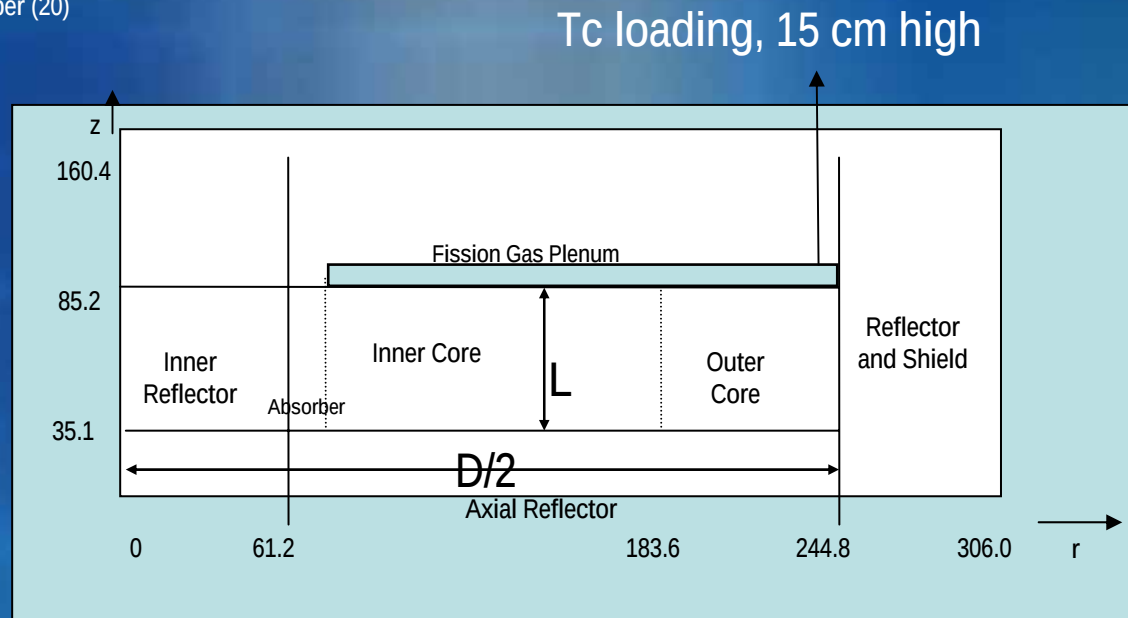
System Design Parameters

Thermal Power [MWth]	1,560	Cycle Length [day]	365
Electric Power [MWe]	550	Capacity Factor [%]	90
Thermal Efficiency [%]	35	Fuel Composition	U-TRU-Zr (57.2-31.9-10.9)
Coolant	Pb-Bi	Smeared Density [%]	67 (≤ 73)
Control Assembly	B ₄ C	Enrichment Zones	2
EFPD [day]	330	Cladding Material	HT-9

Reactor Core Design

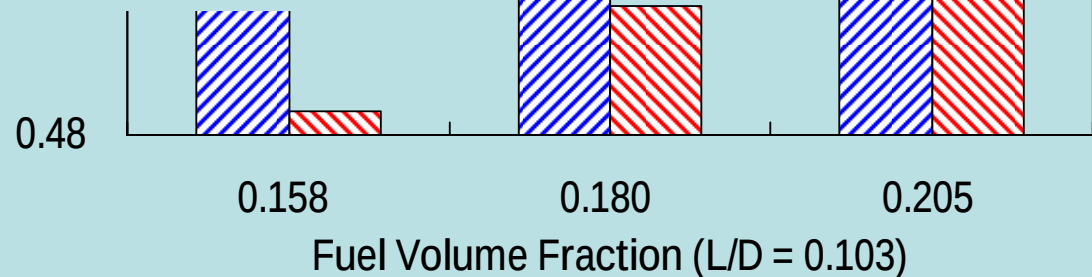
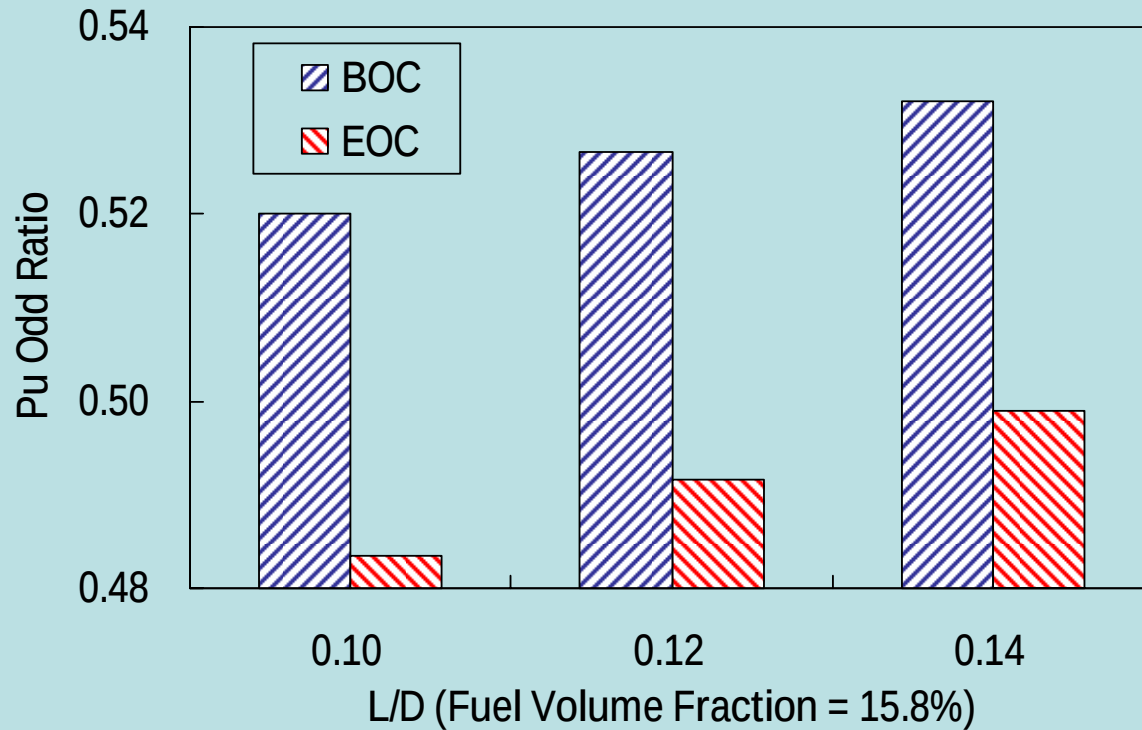


Cross-sectional View



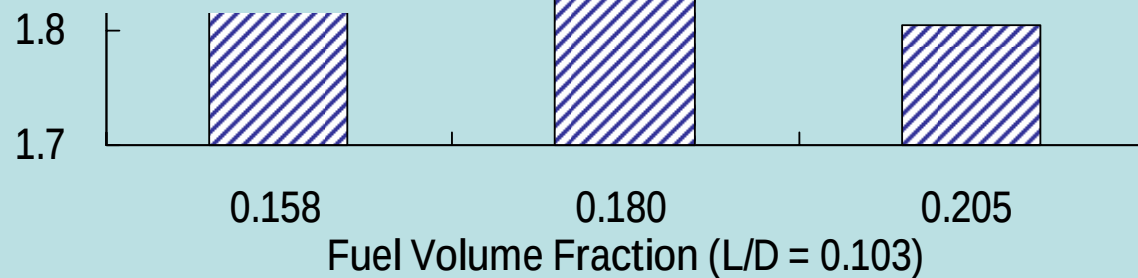
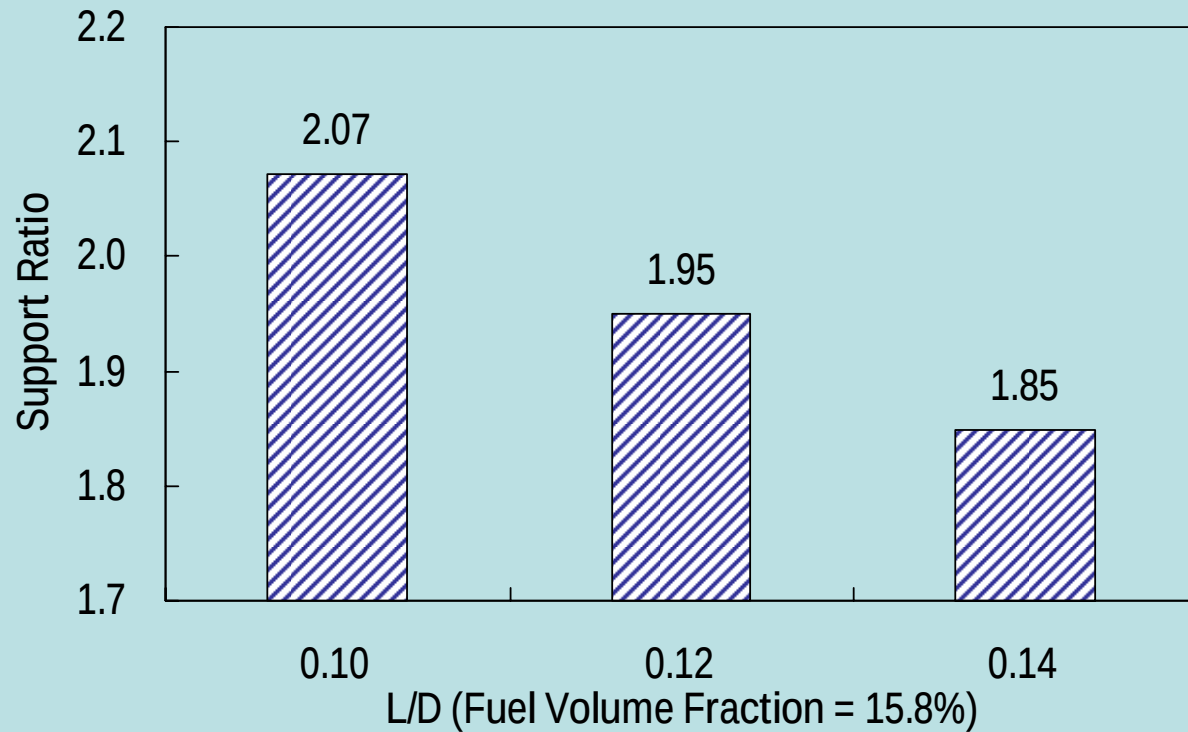
Side View (unit: cm)

Proliferation-Resistance



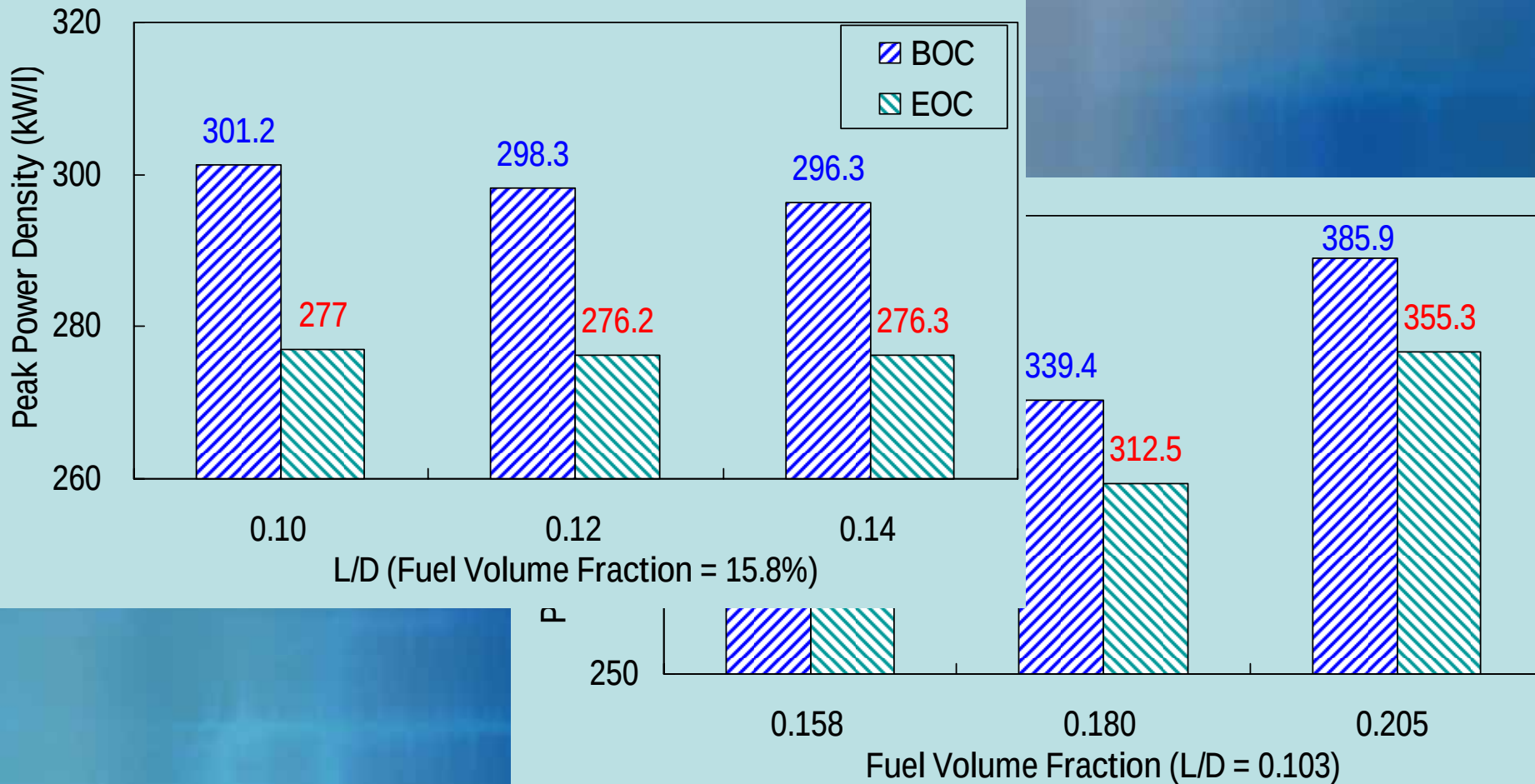
Goal for OR(<0.5) is achieved at low L/D and fuel volume fraction

Environment-Friendliness



Goal for SR(>2.0) is achieved at low L/D and fuel volume fraction

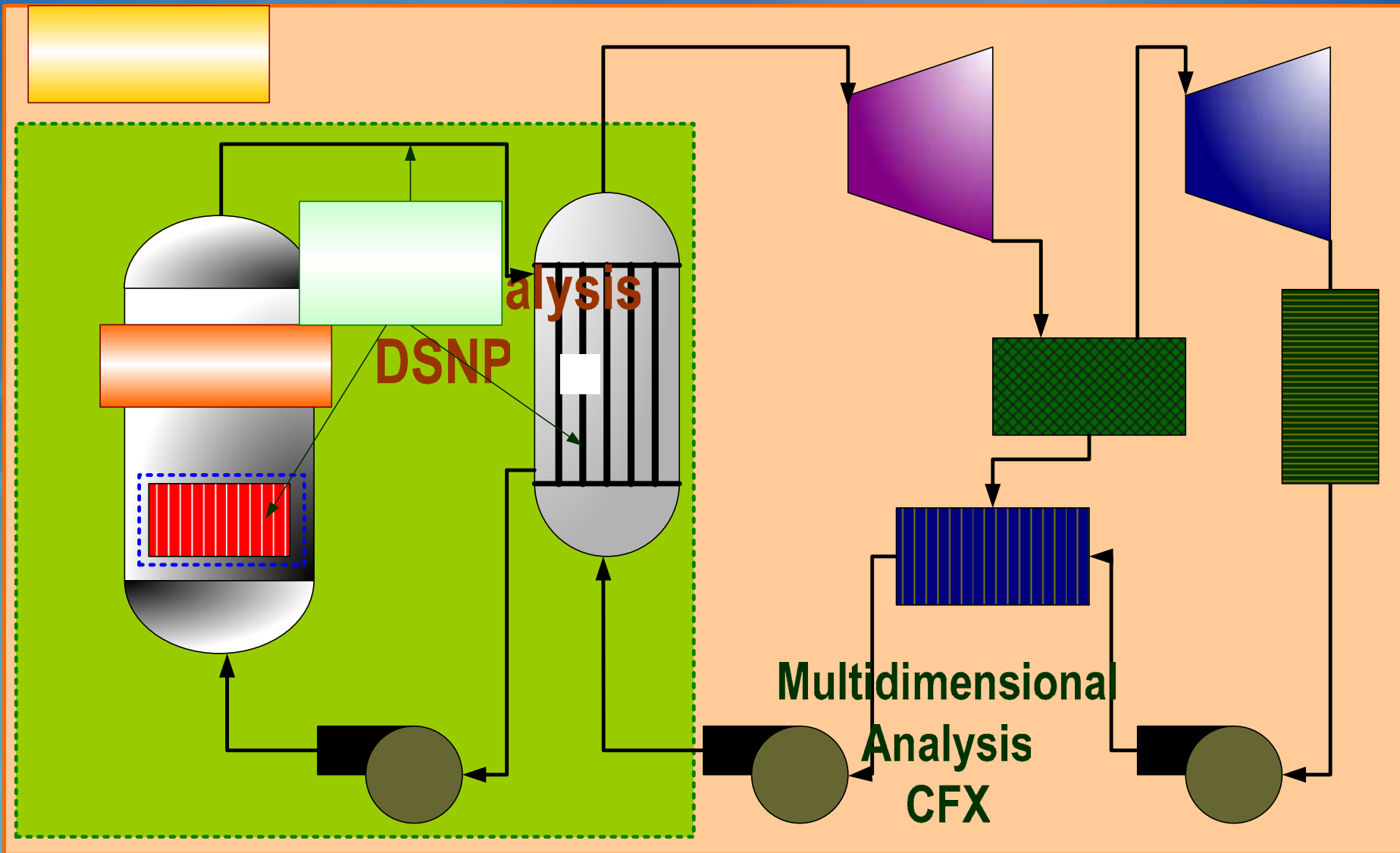
Accident-Tolerance



- Peak power density is low at 50% of the current Na-cooled reactor
- Peak power density decreases with fuel volume fraction

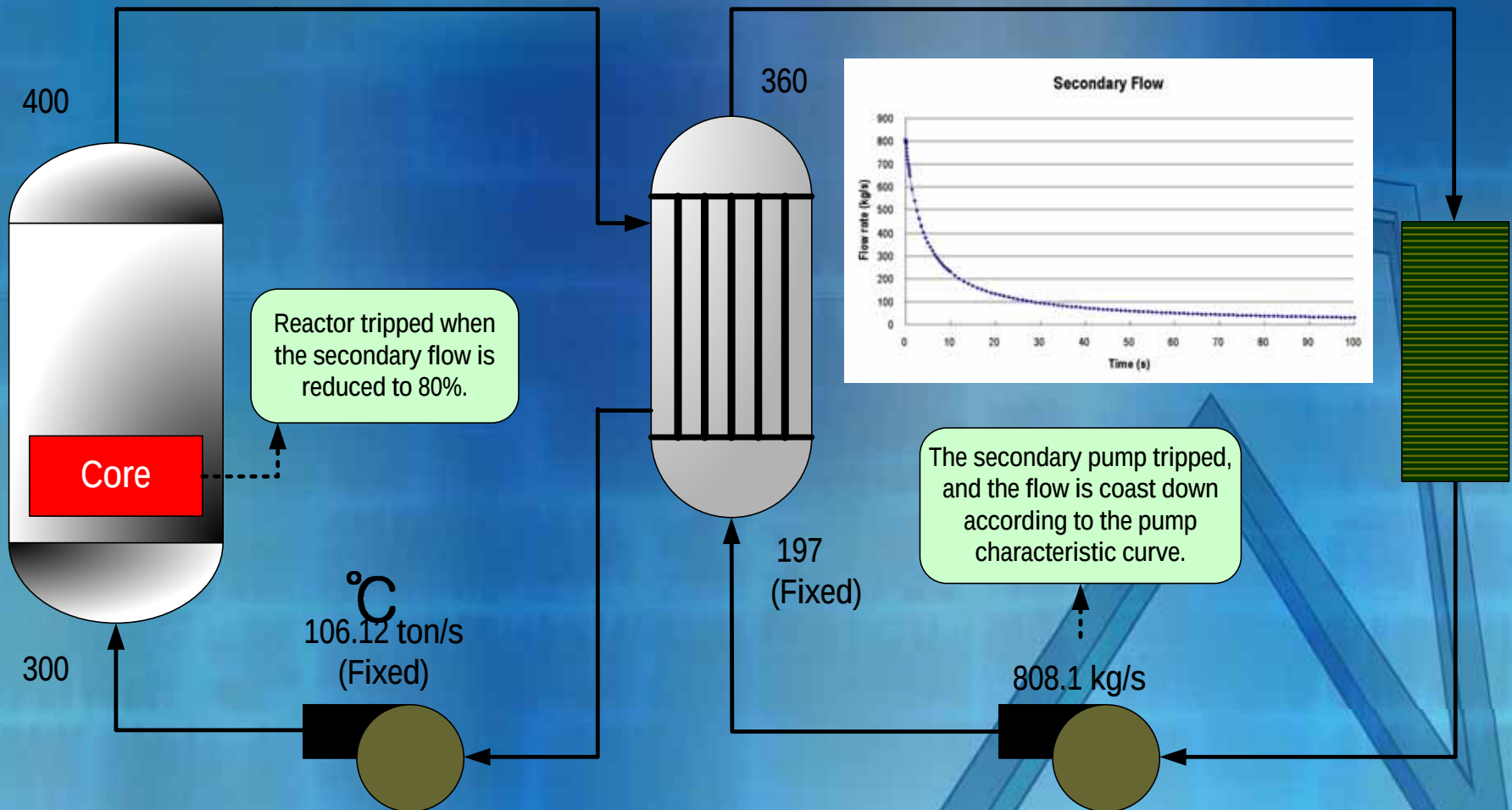
Transient Analysis

Analysis Domain



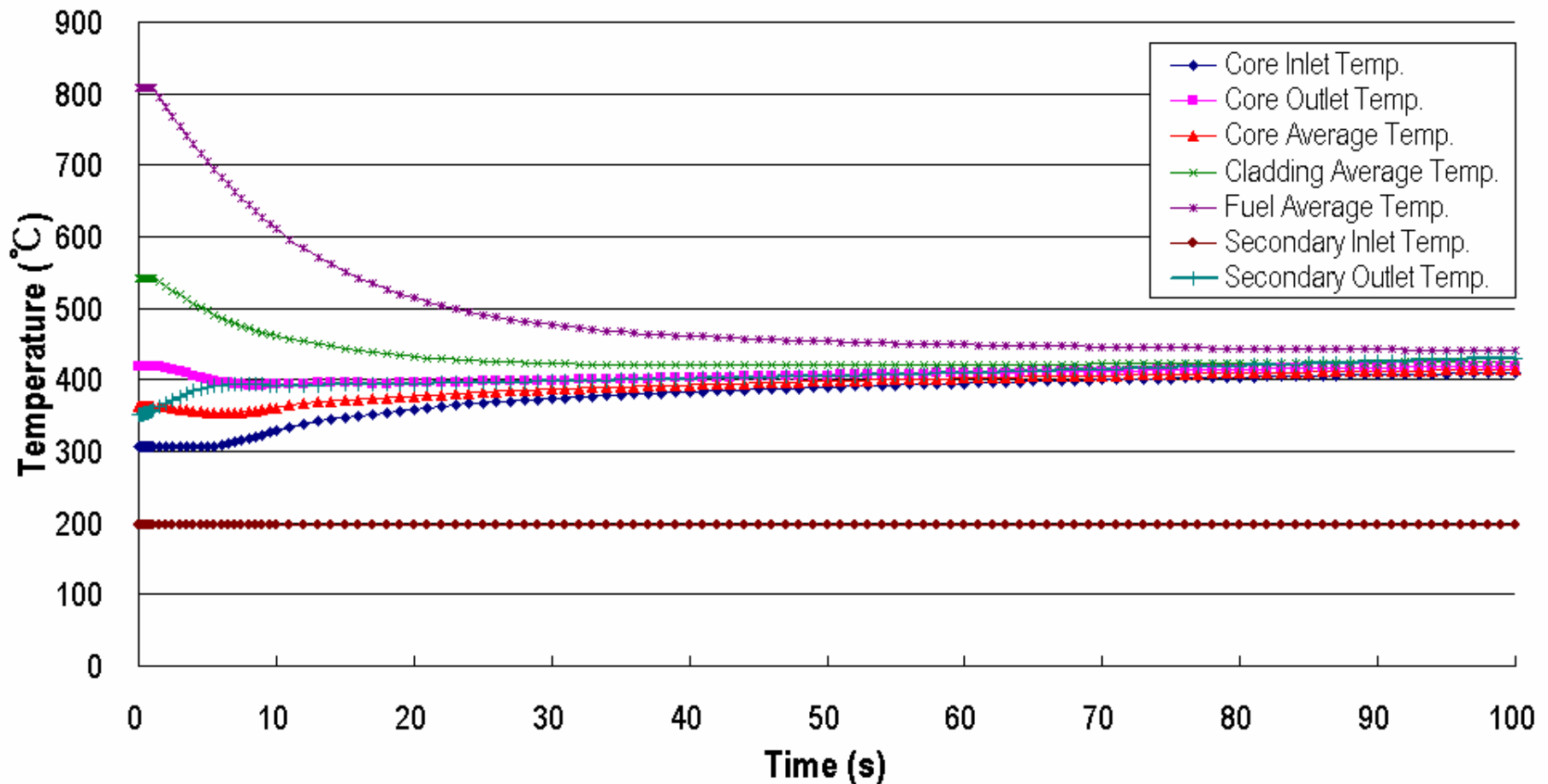
Problem Definition

Loss of Heat Sink



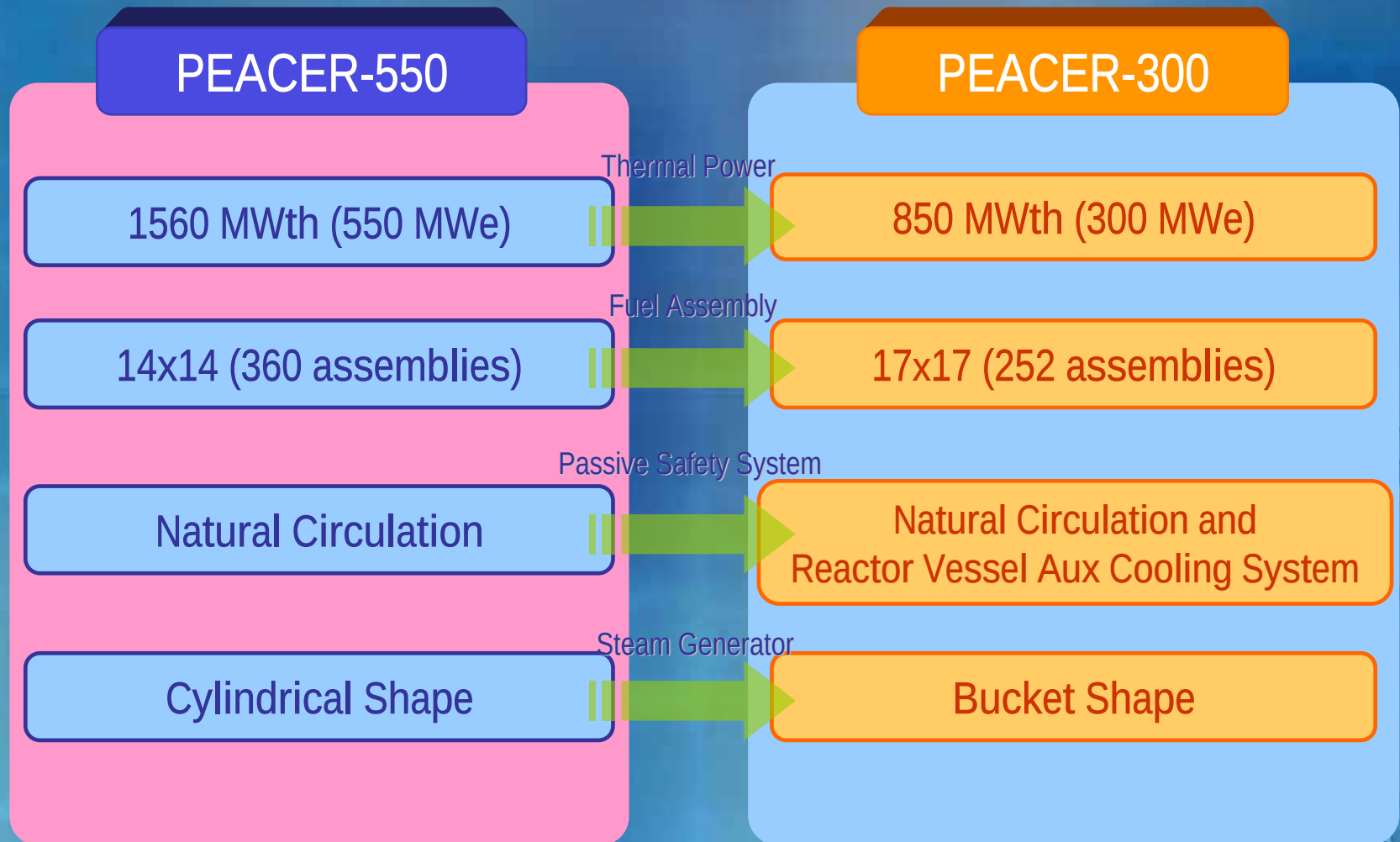
Temperature Transient

Temperature Transient

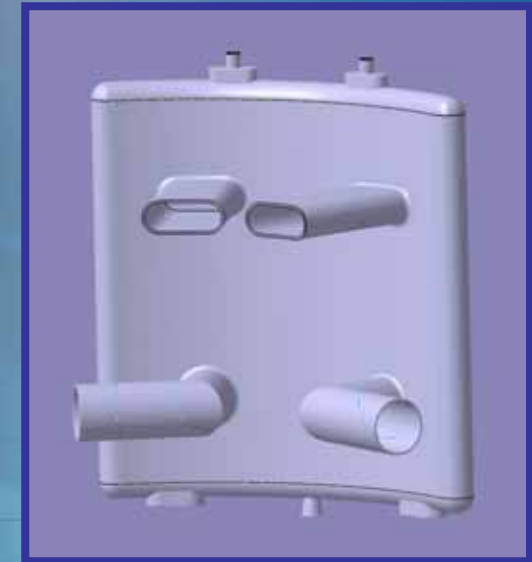
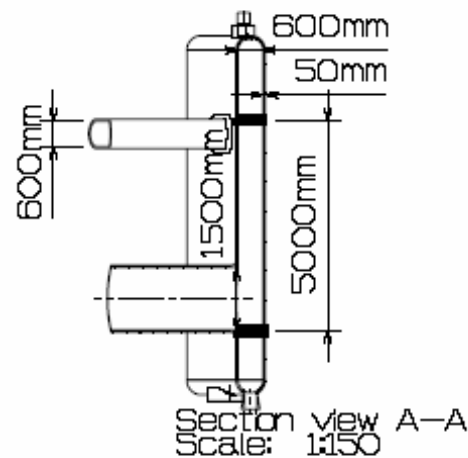
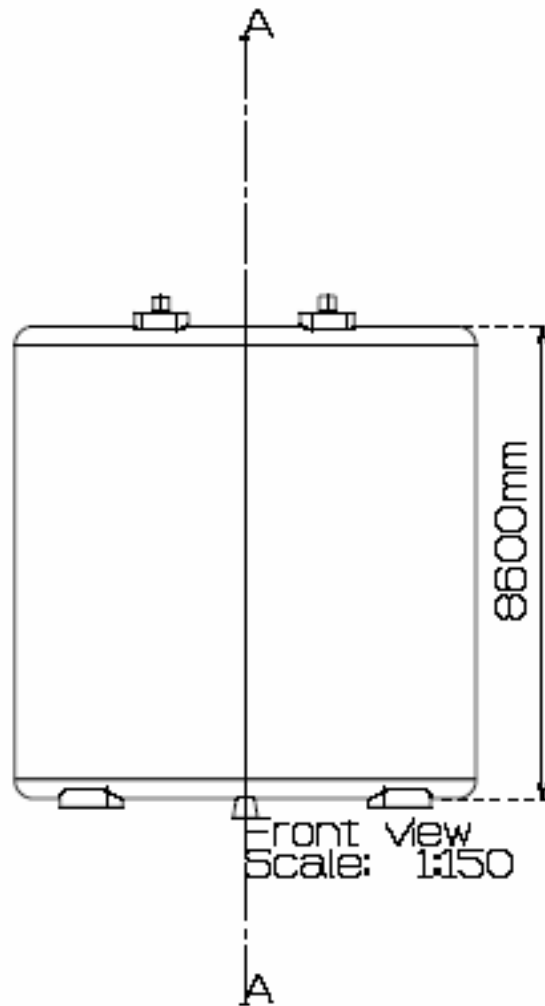


Design Shakedown

PEACER-300 Design

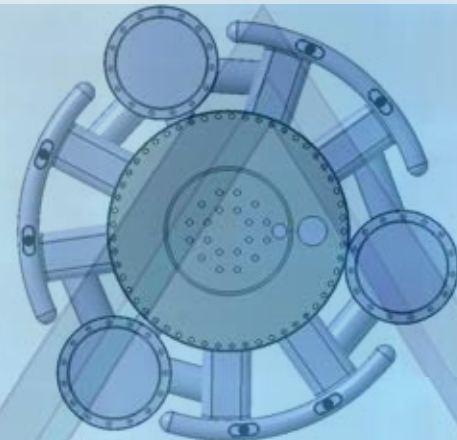
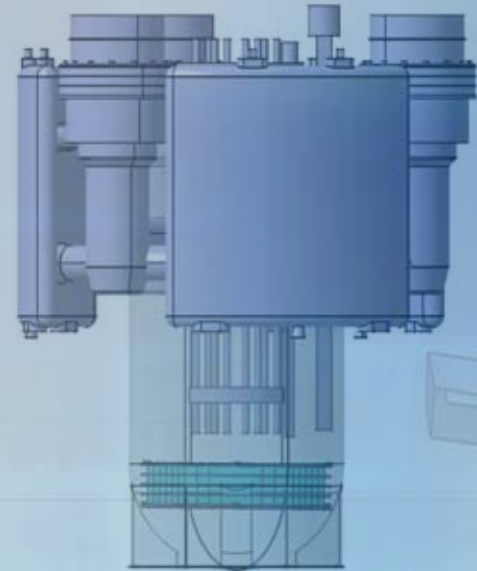
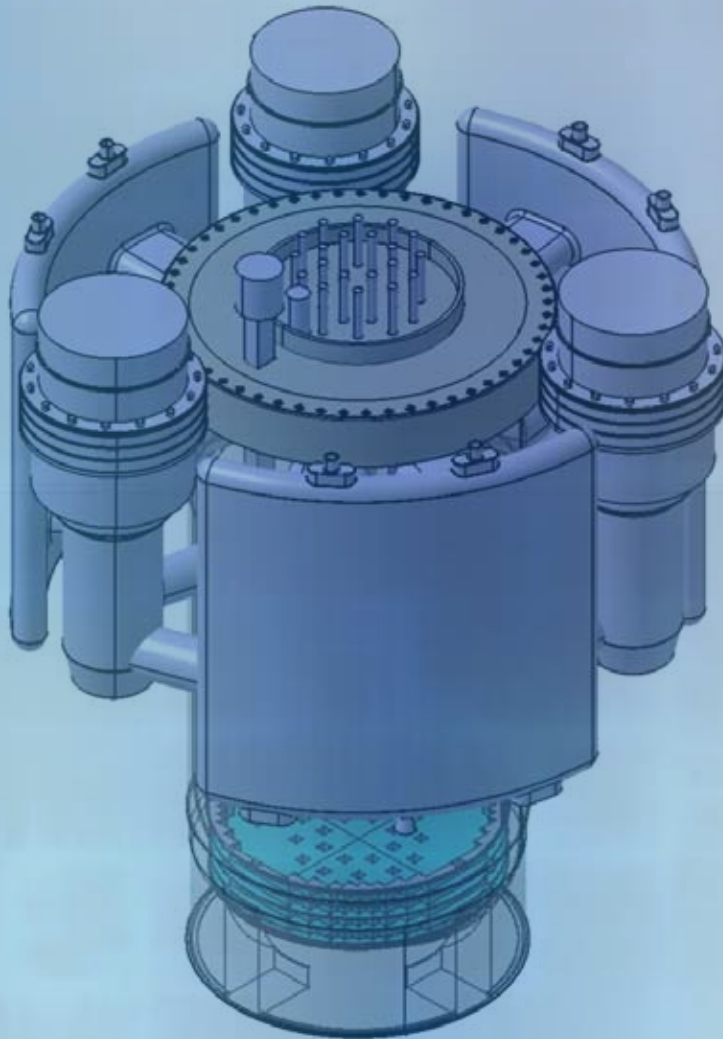


Schematic of Steam Generator

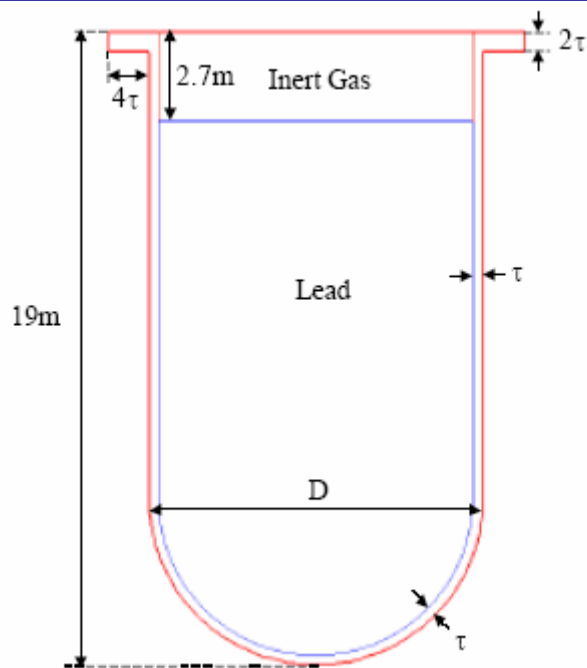


Geometry	Design Value
Pressure [MPa]	8
Number of Loops	3
Number of Tubes per Unit	9,853
Tube Length [m]	5
P/D, Tube Outer/Inner Diameter [mm]	1.2, 20/16
Mass Flow Rate [kg/s]	19,353
Feedwater Mass Flow Rate [kg/s]	146

PEACER-300 Primary System

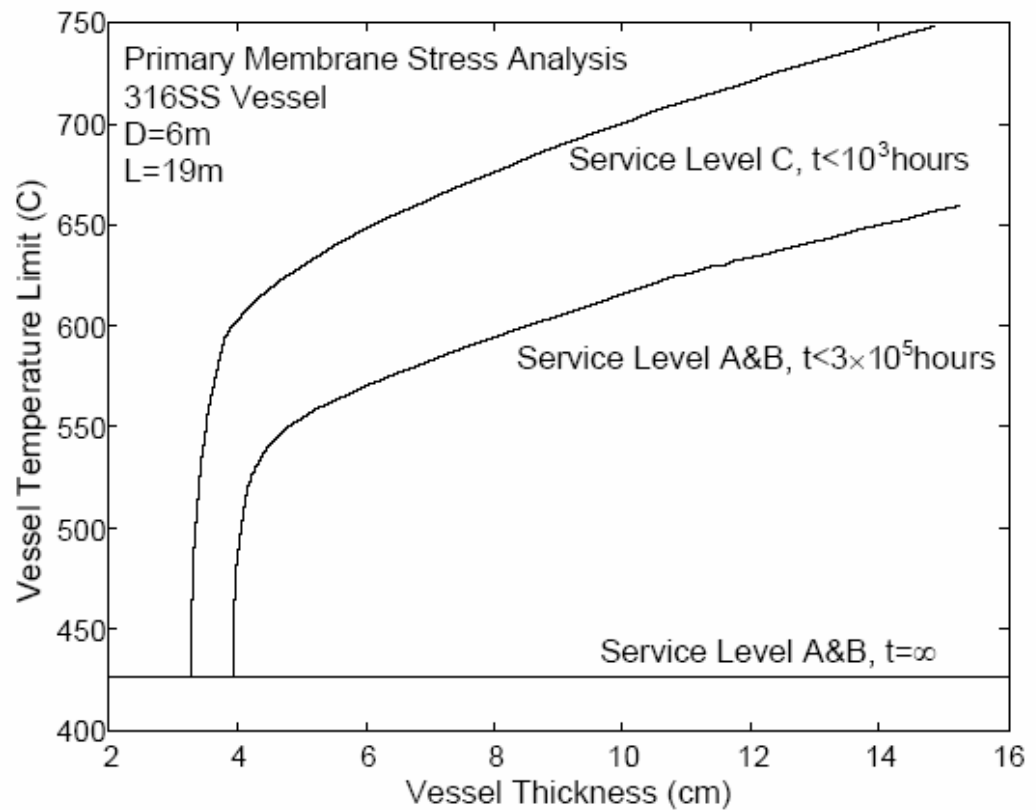


Thermal Limits of Guard Vessel

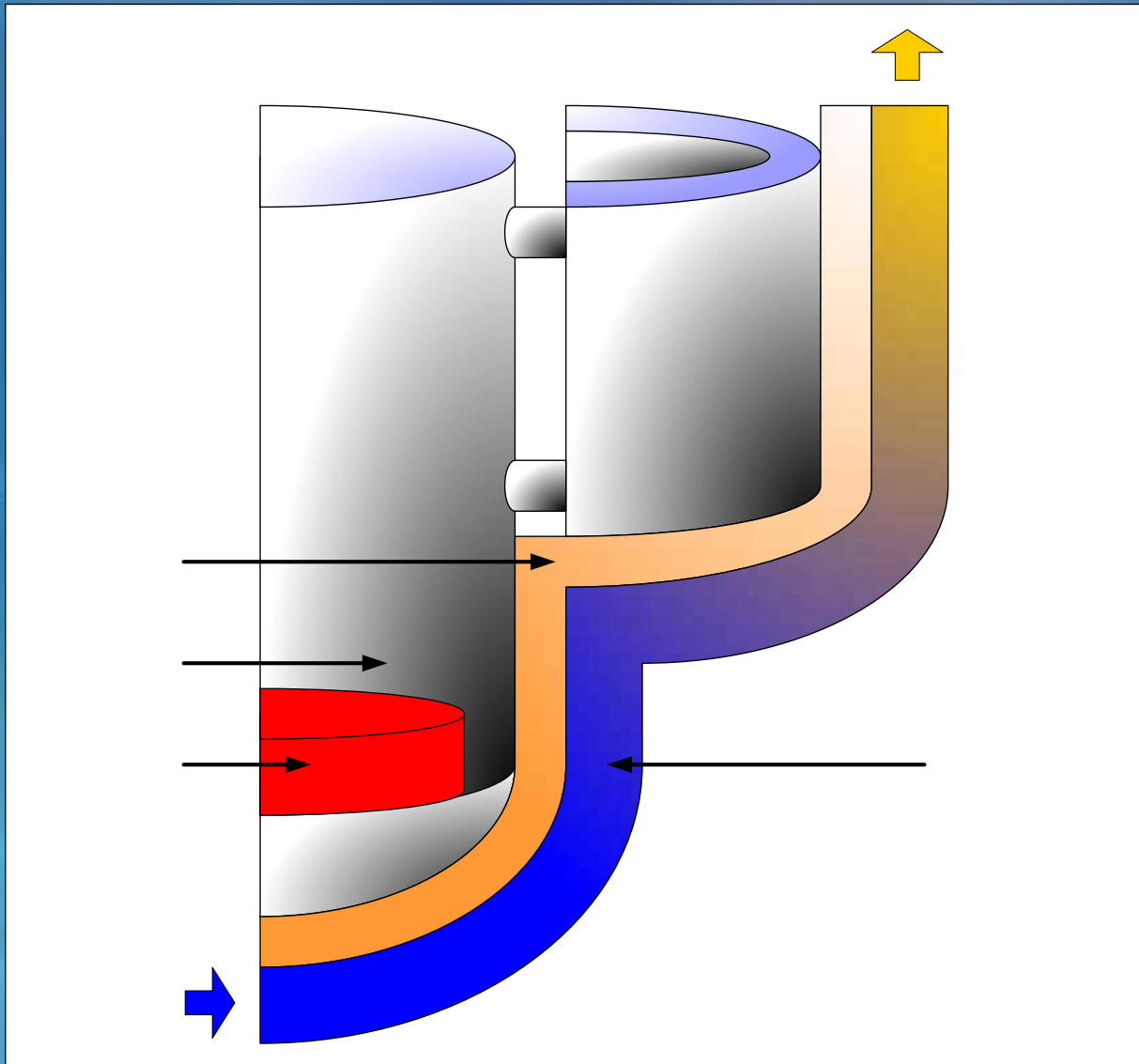


The ASME Code

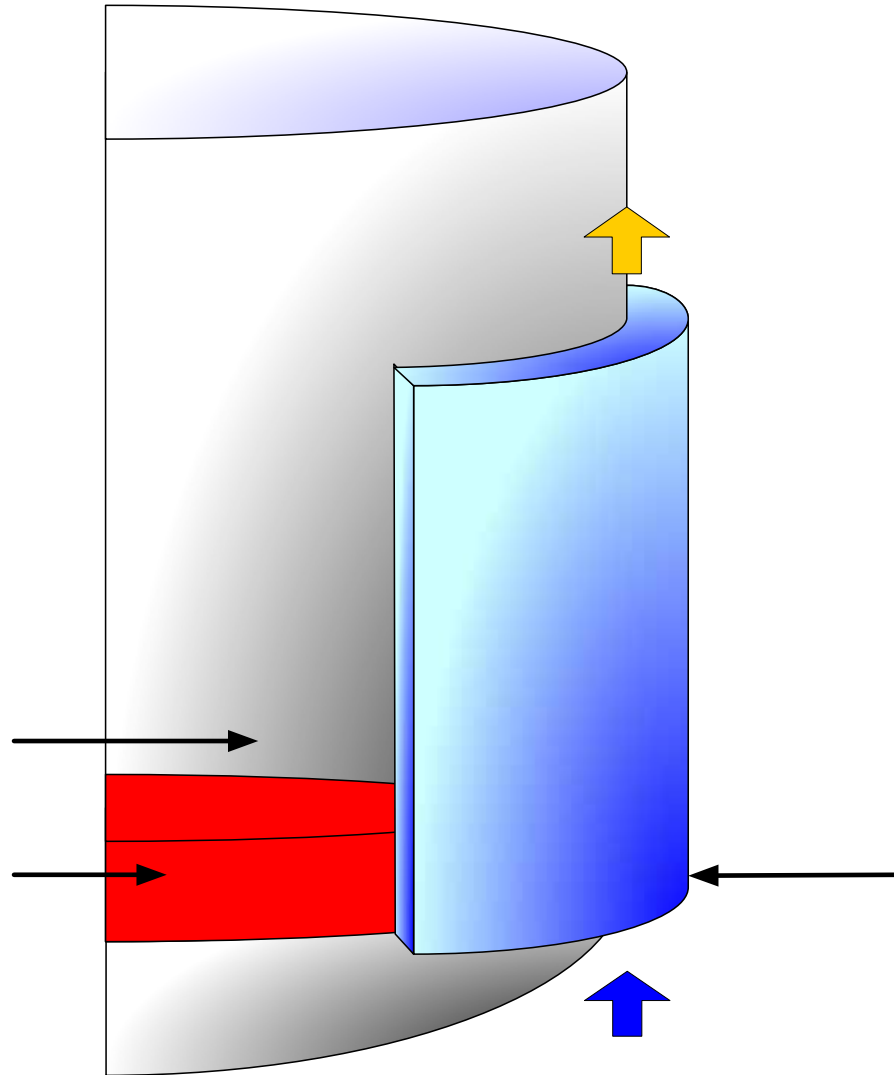
The ASME Boiler and Pressure Vessel Code
Section III, Division 1, Section NH (Class 1
Component in Elevated Temperature Service)



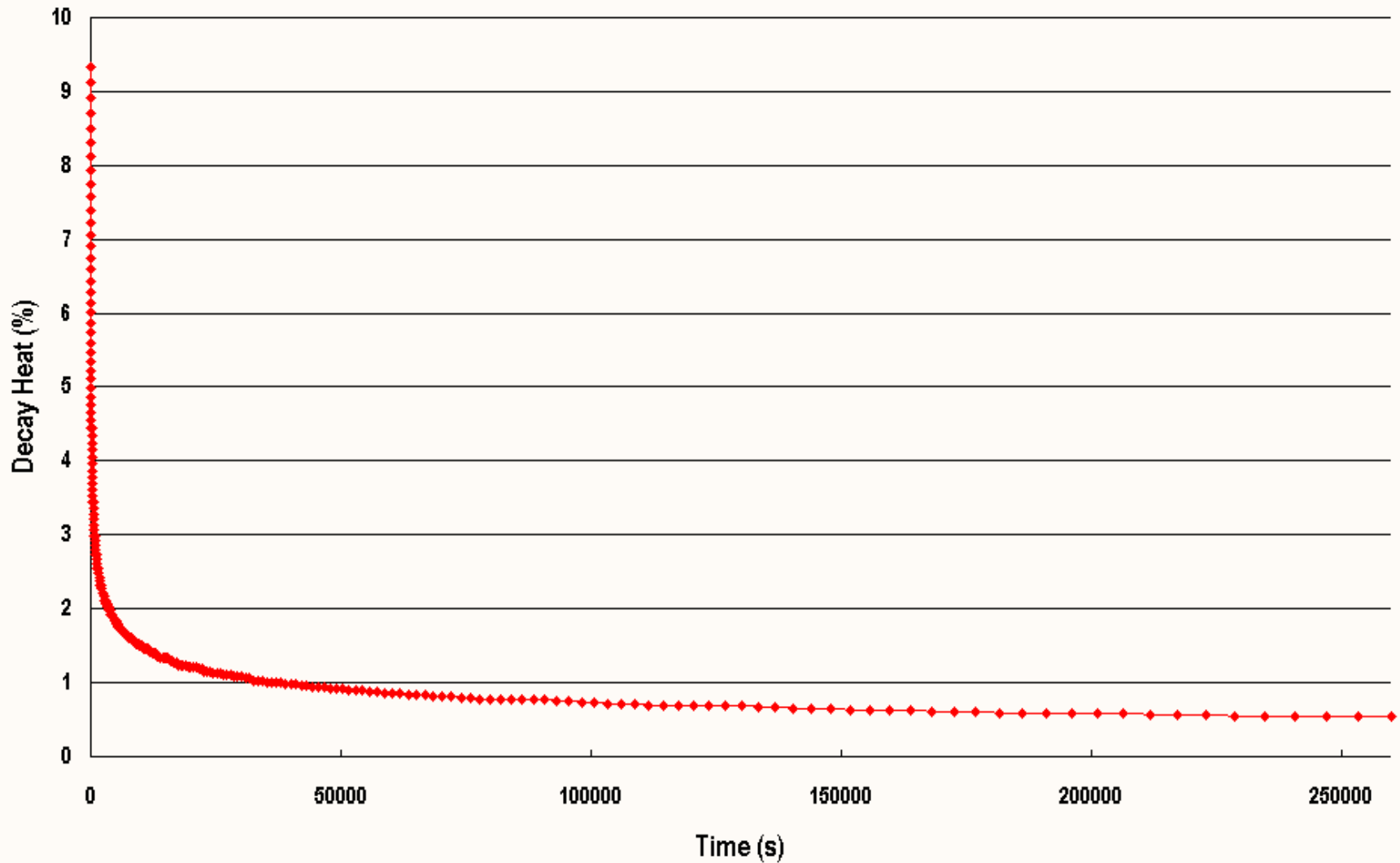
Air Cooling System Layout



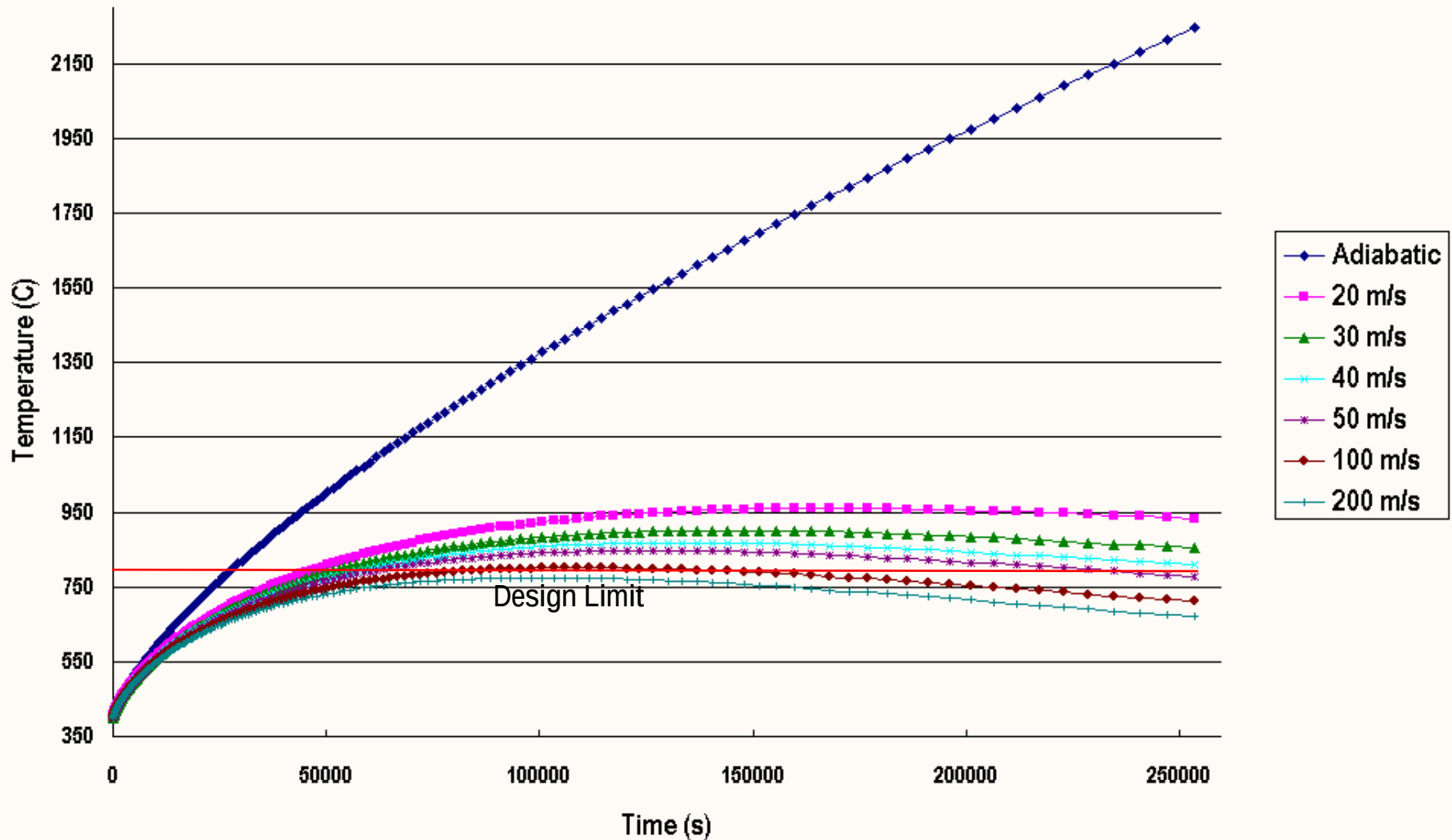
Water Pad System Layout



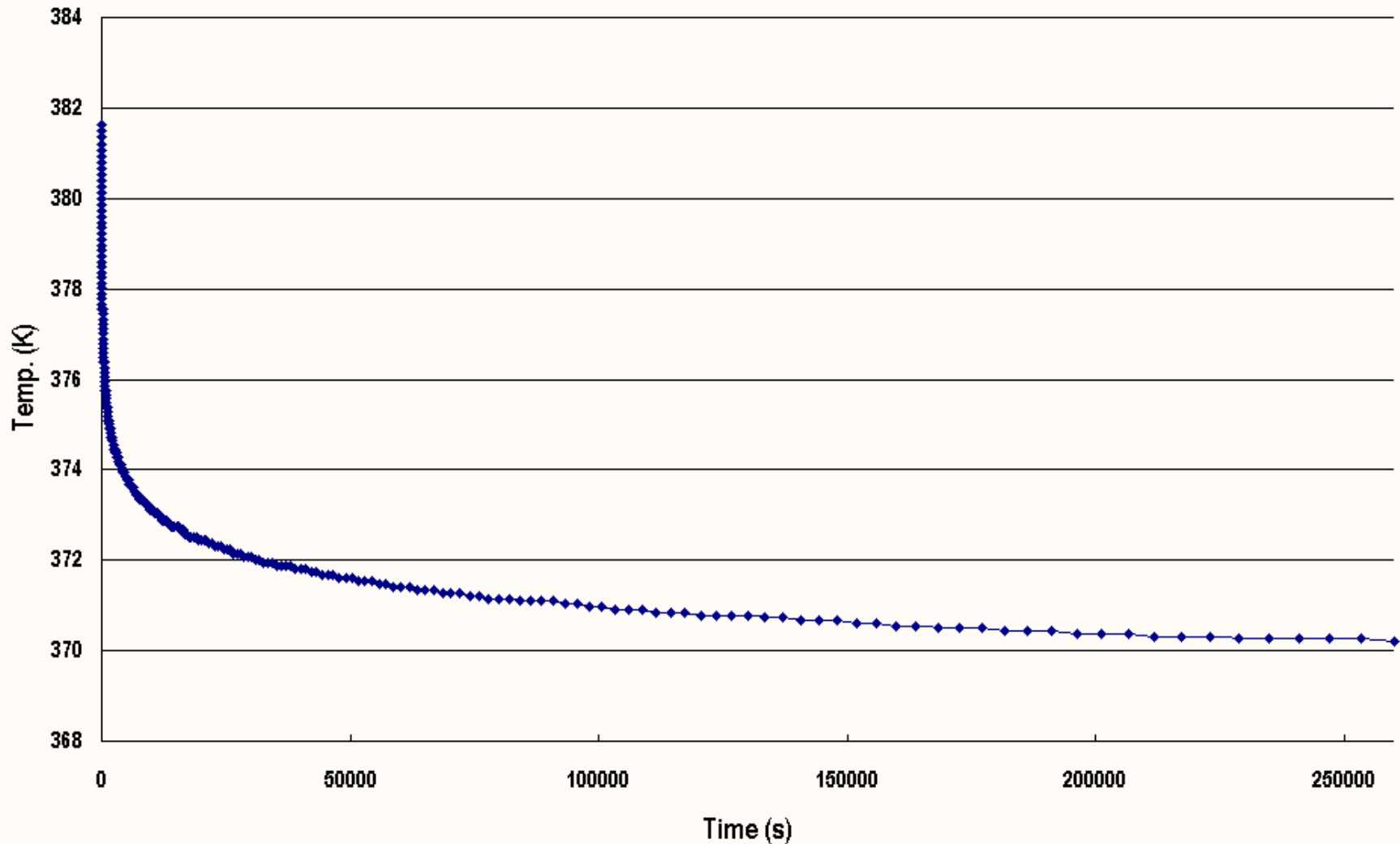
Decay Heat Transient



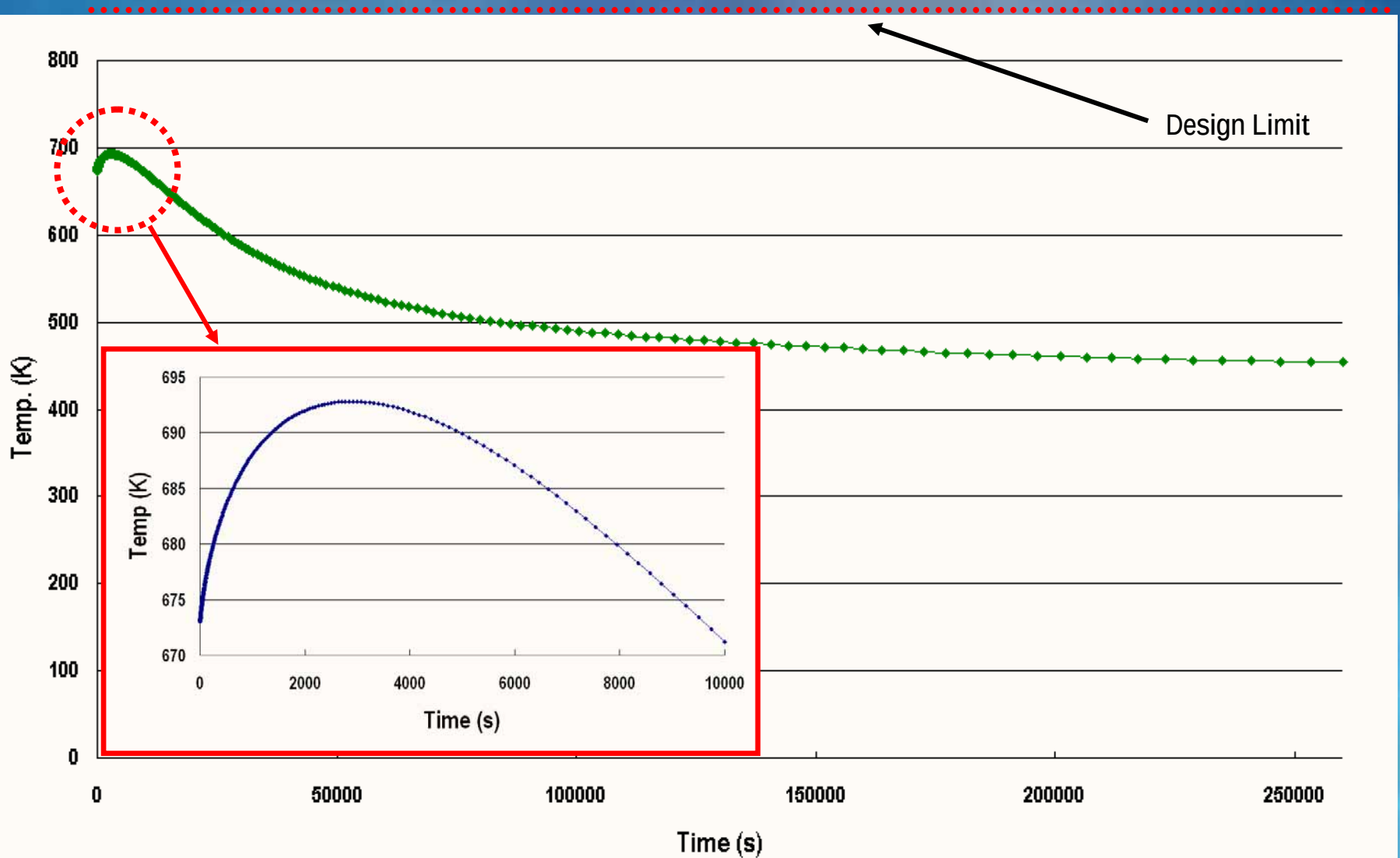
Air Cooling System Efficiency



Reactor Vessel Outer Temperature

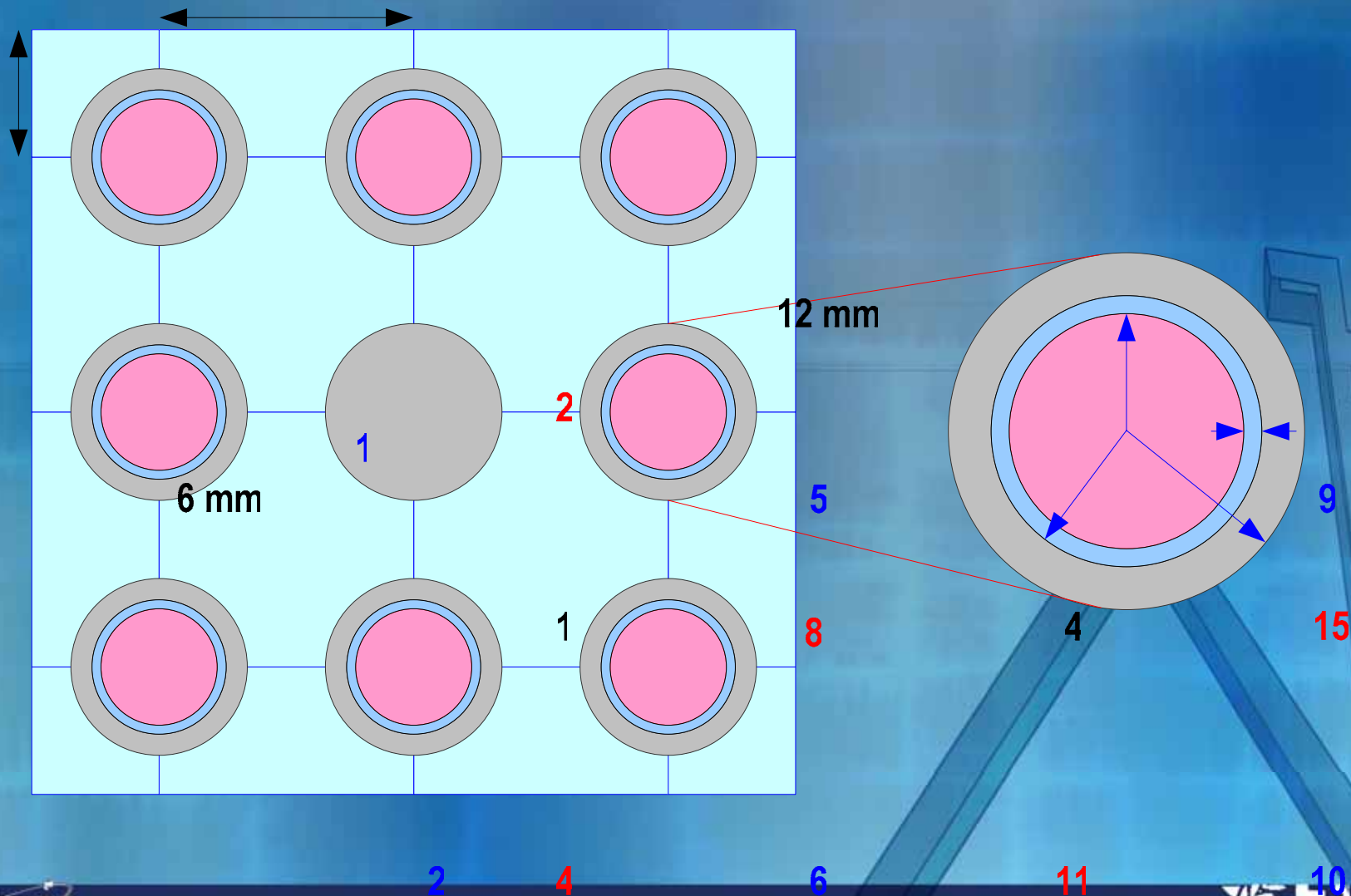


Reactor Vessel Inner Temperature



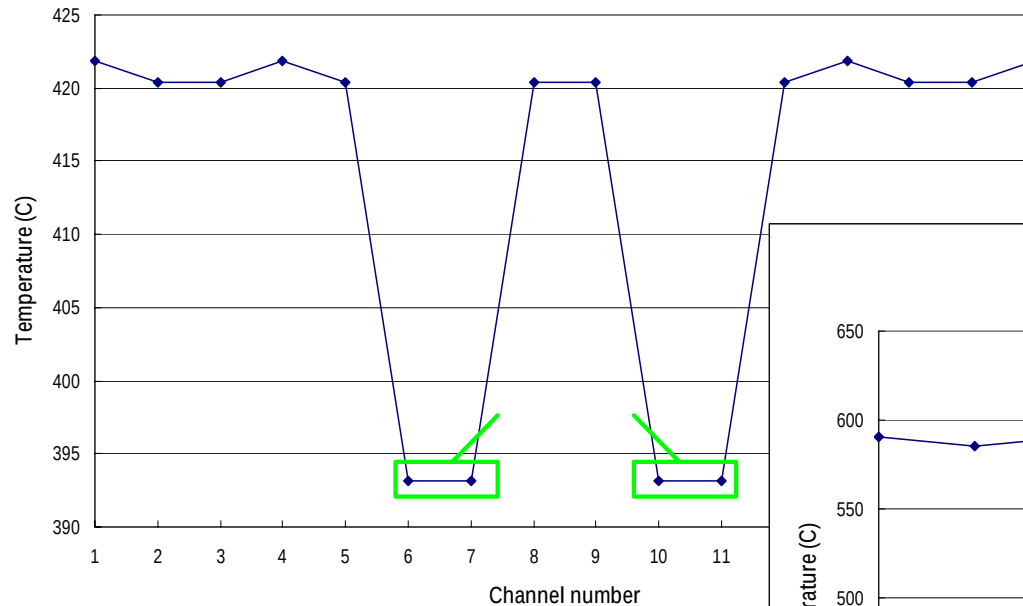
Subchannel Analysis

Region of Interest (3x3)

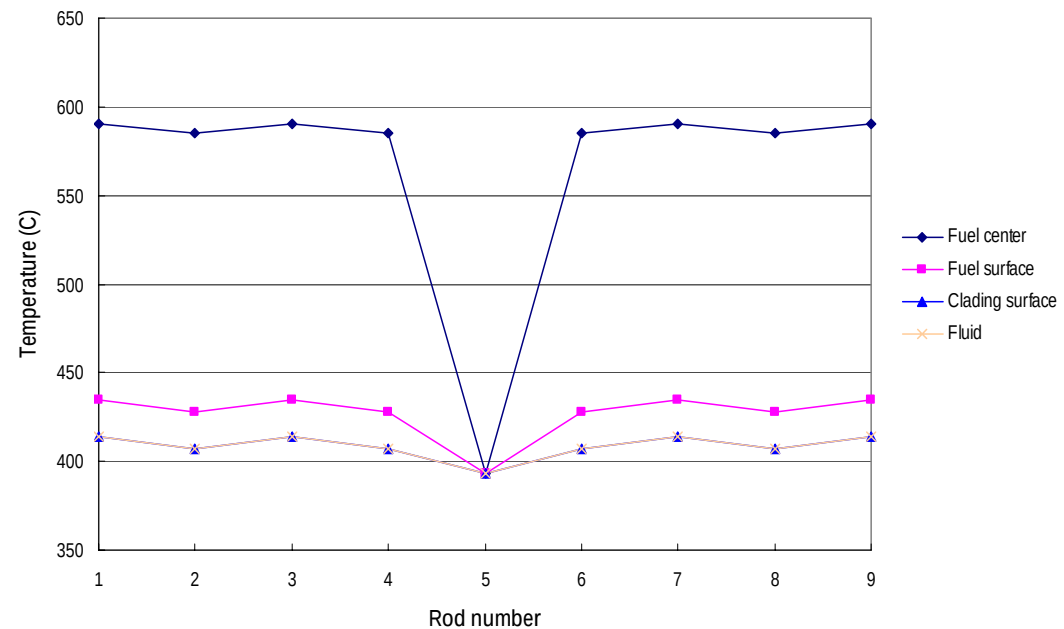


MATRA Computational Results (3x3)

Coolant channel exit temperature distribution

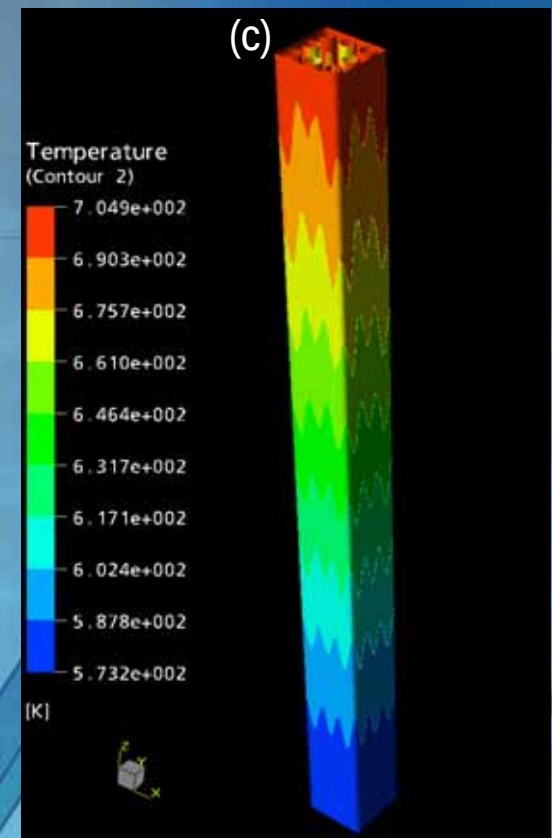
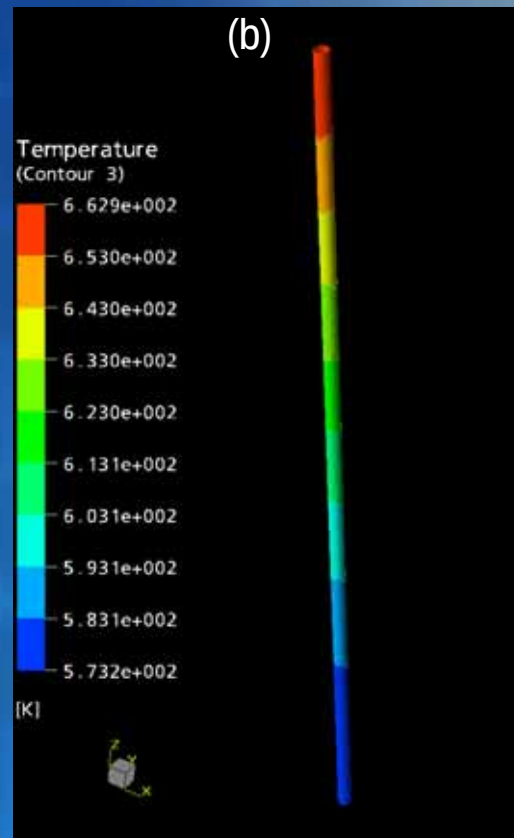
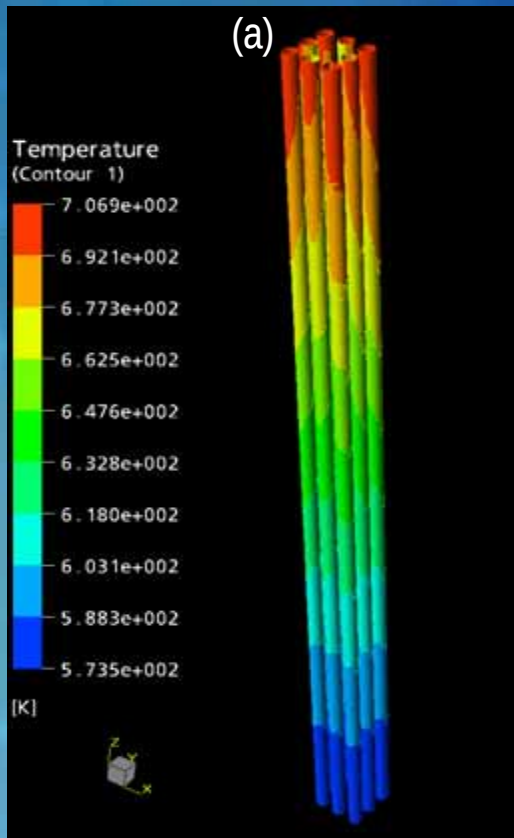


Fuel rod maximum temperature distribution



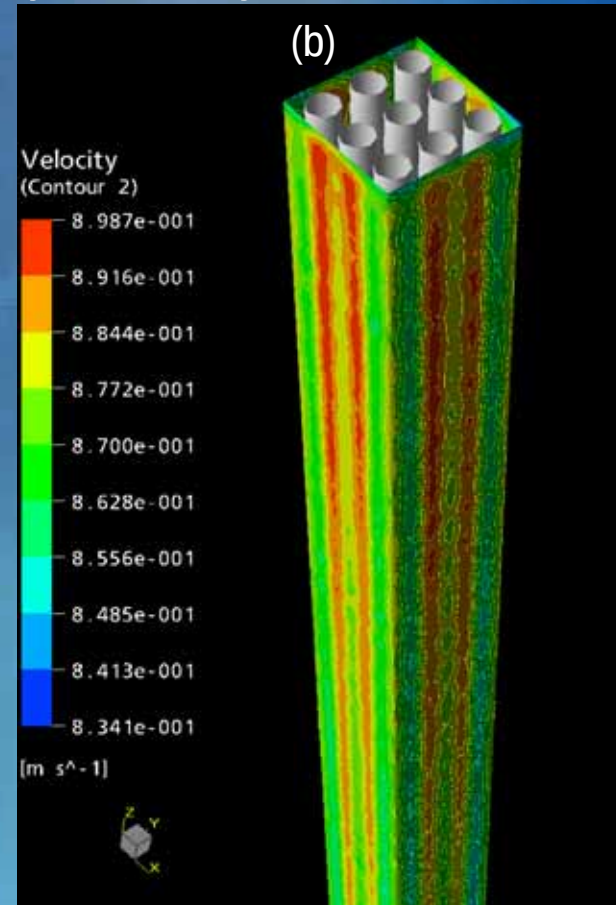
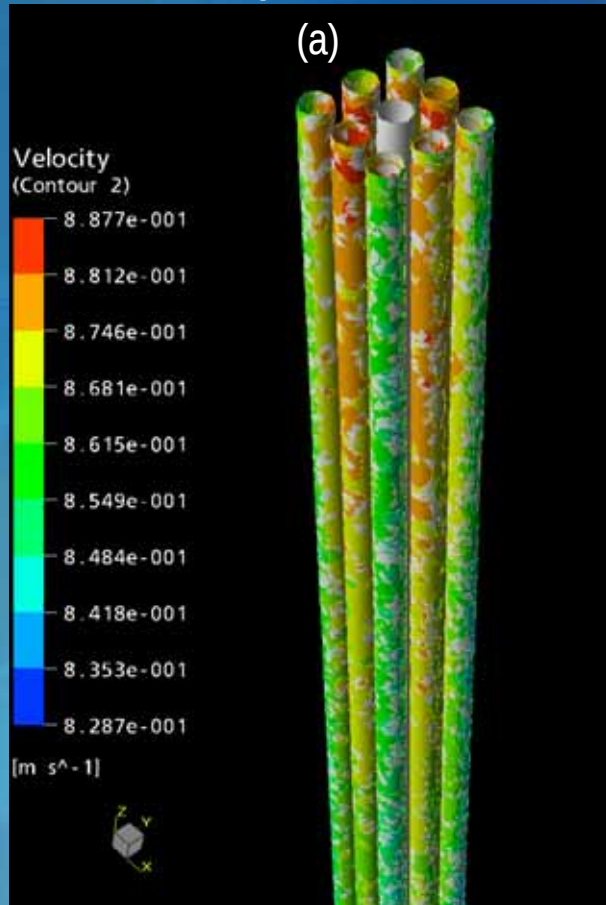
CFX Numerical Results (3x3)

- Coolant temperature on fuel rod surface and at boundary
 - (a) Coolant temperature on fuel rod surface
 - (b) Coolant temperature on a skeleton surface
 - (c) Coolant temperature at symmetry boundary



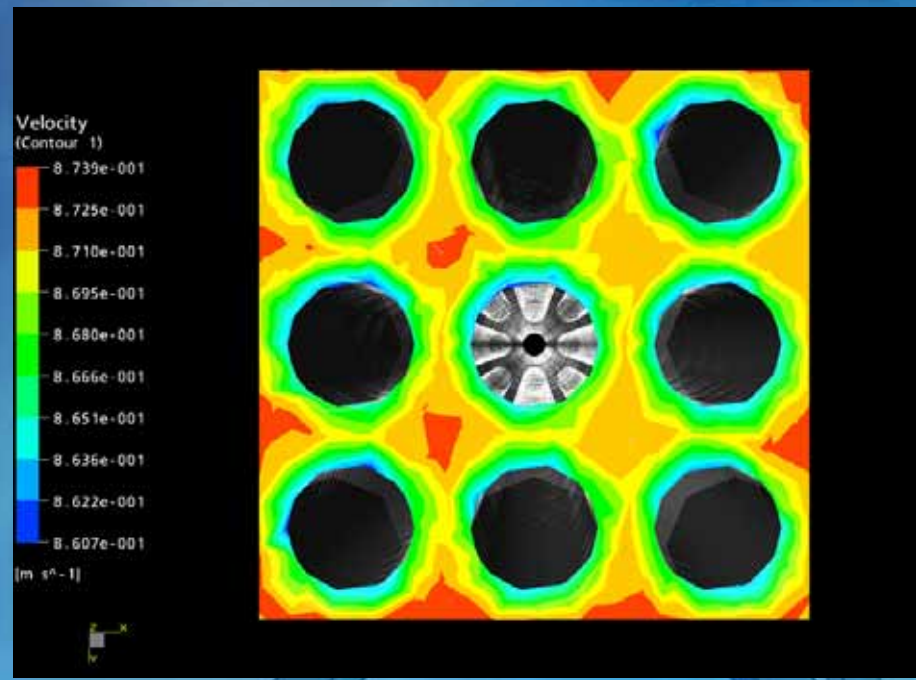
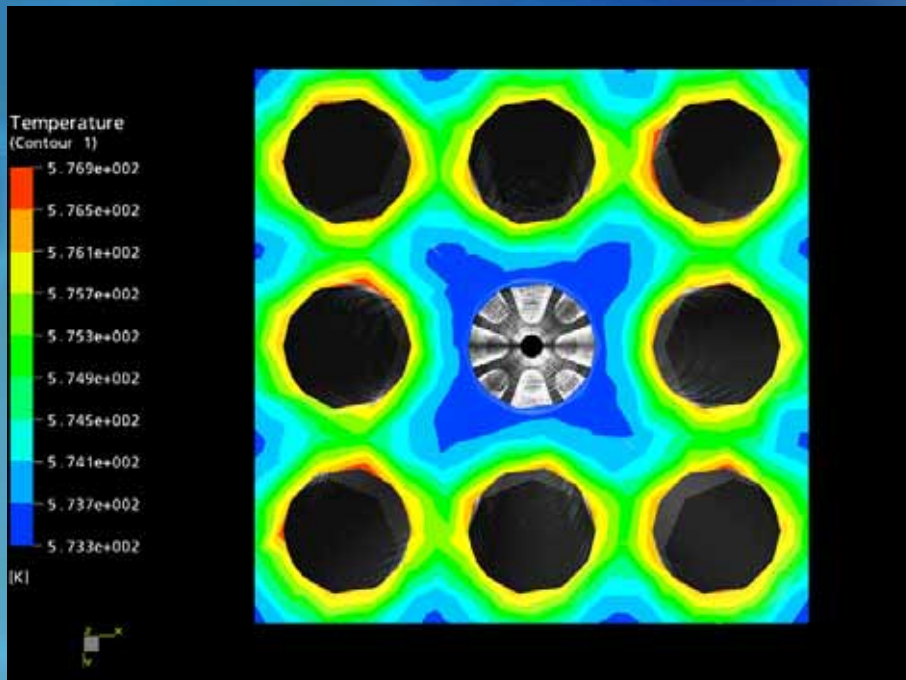
CFX Numerical Results (3x3)

- Coolant velocity on fuel rod surface and at boundary
 - (a) Axial velocity distribution on fuel rod surface
 - (b) Axial velocity distribution at symmetry boundary



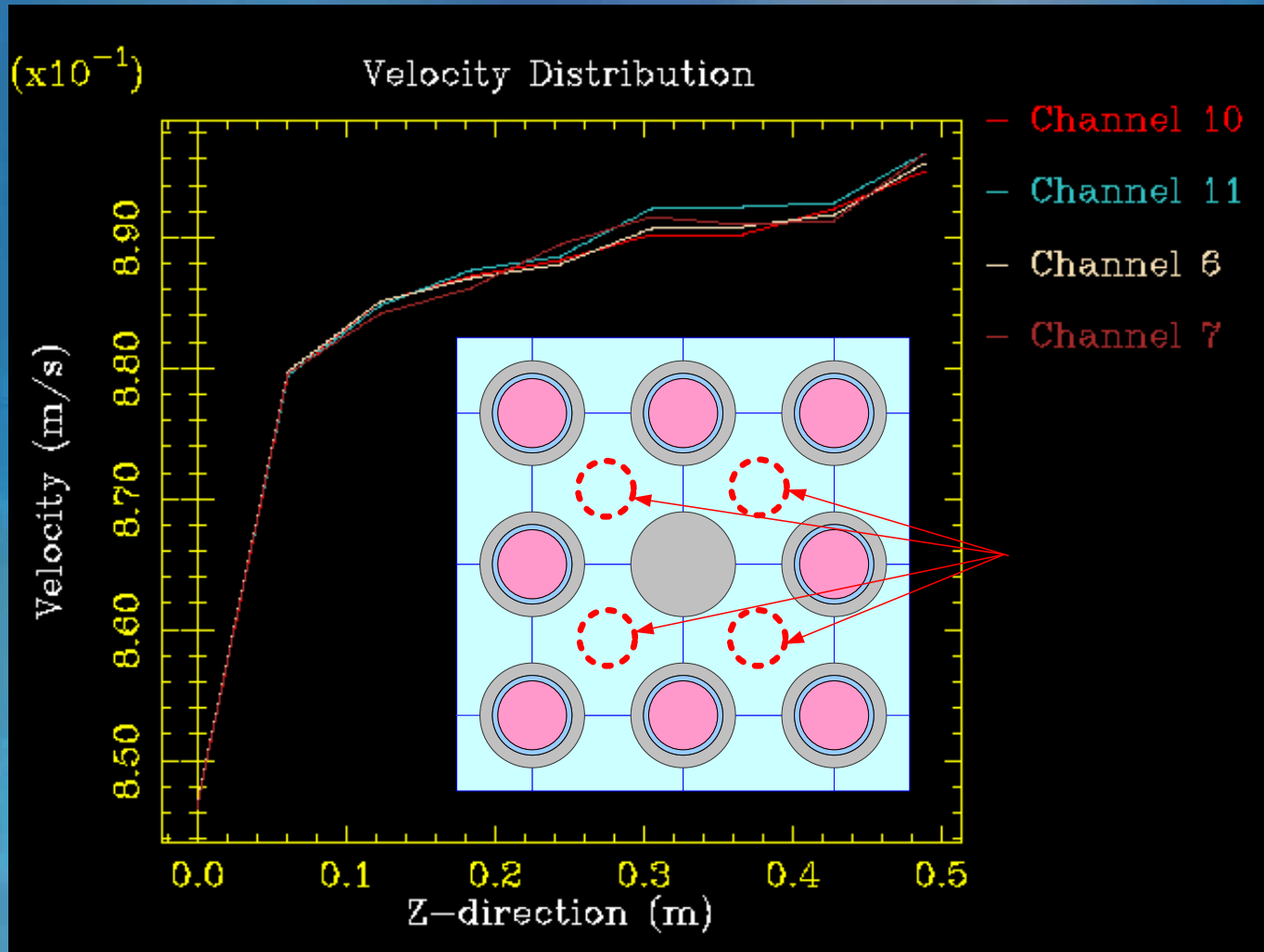
CFX Numerical Results (3x3)

- Temperature and velocity distributions in a horizontal section at $z = 0\text{m}$ (inlet)
 - Similar temperature and velocity profiles on each fuel rod except skeleton



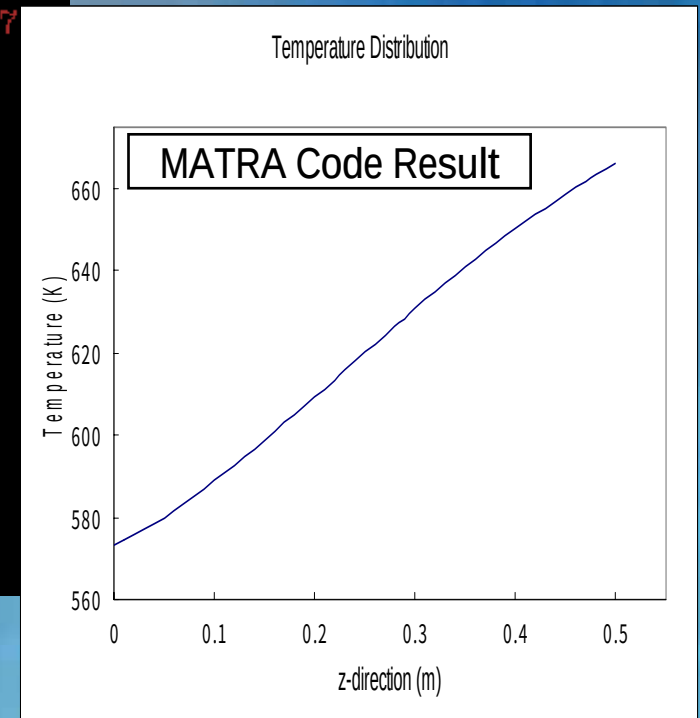
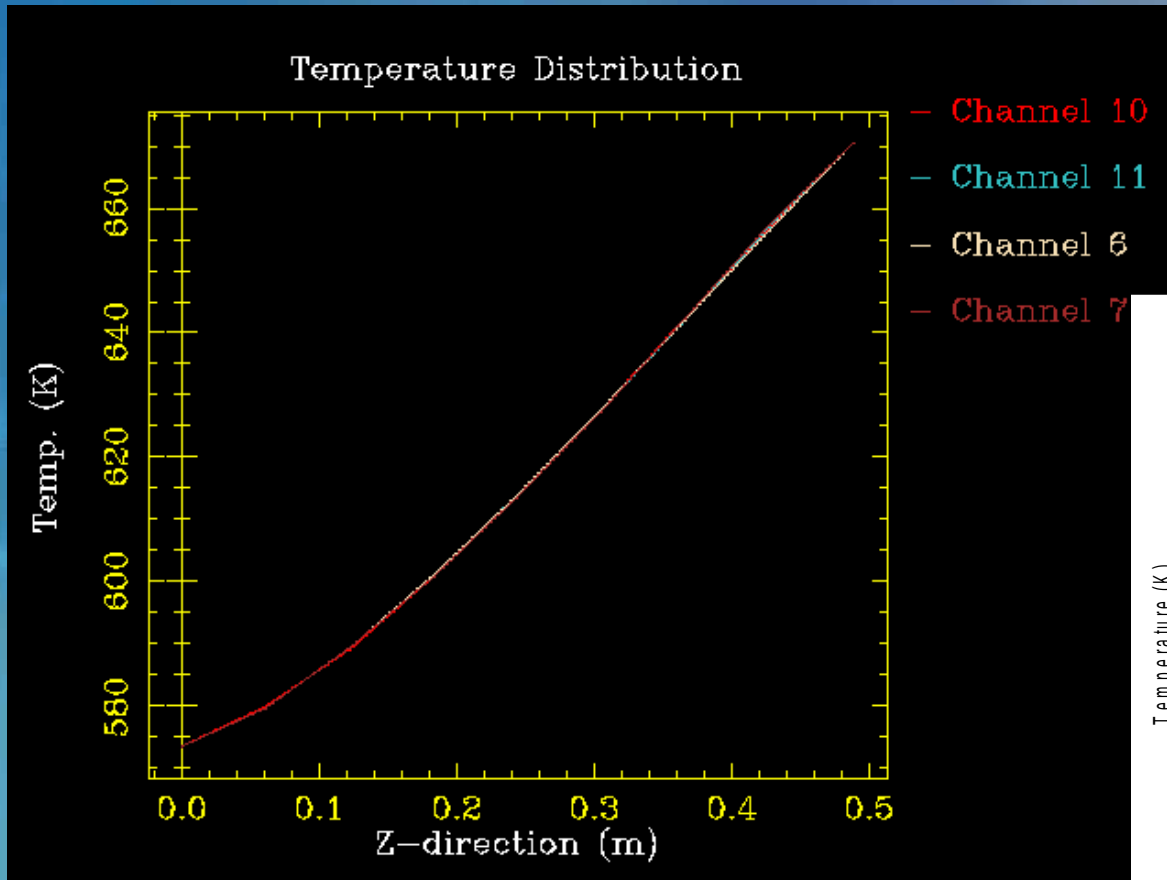
CFX Numerical Results (3x3)

- Axial velocity distribution at center of subchannel

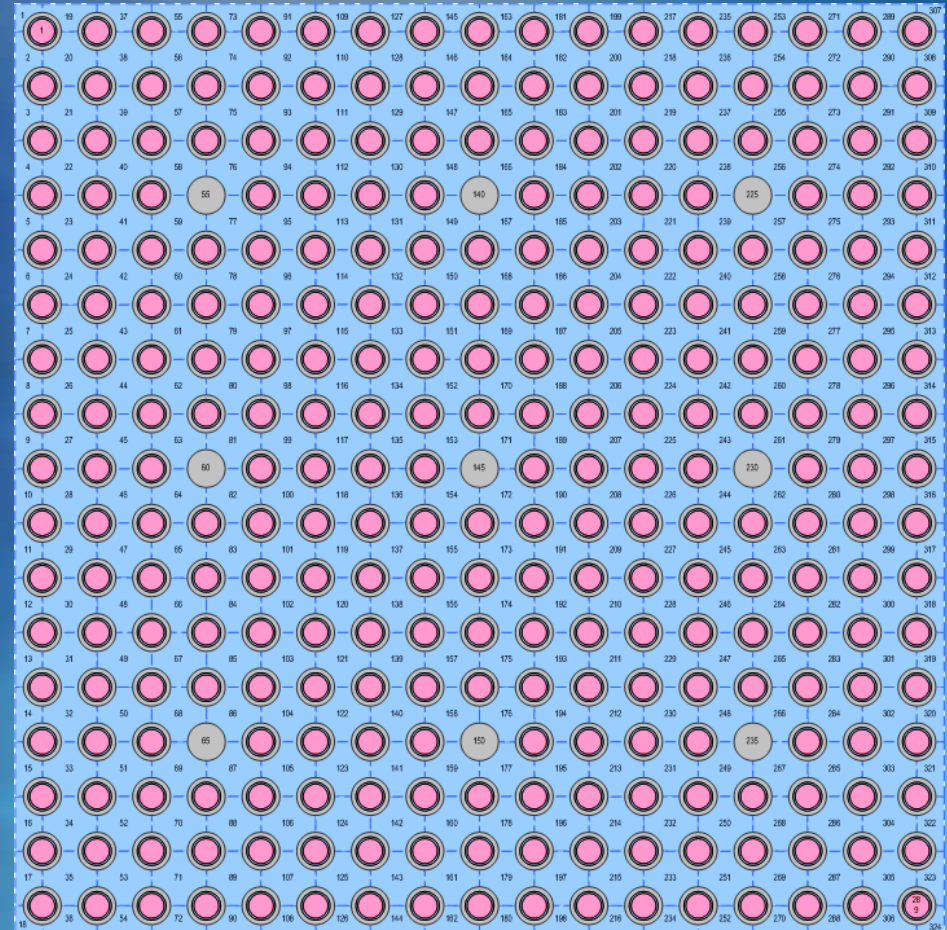
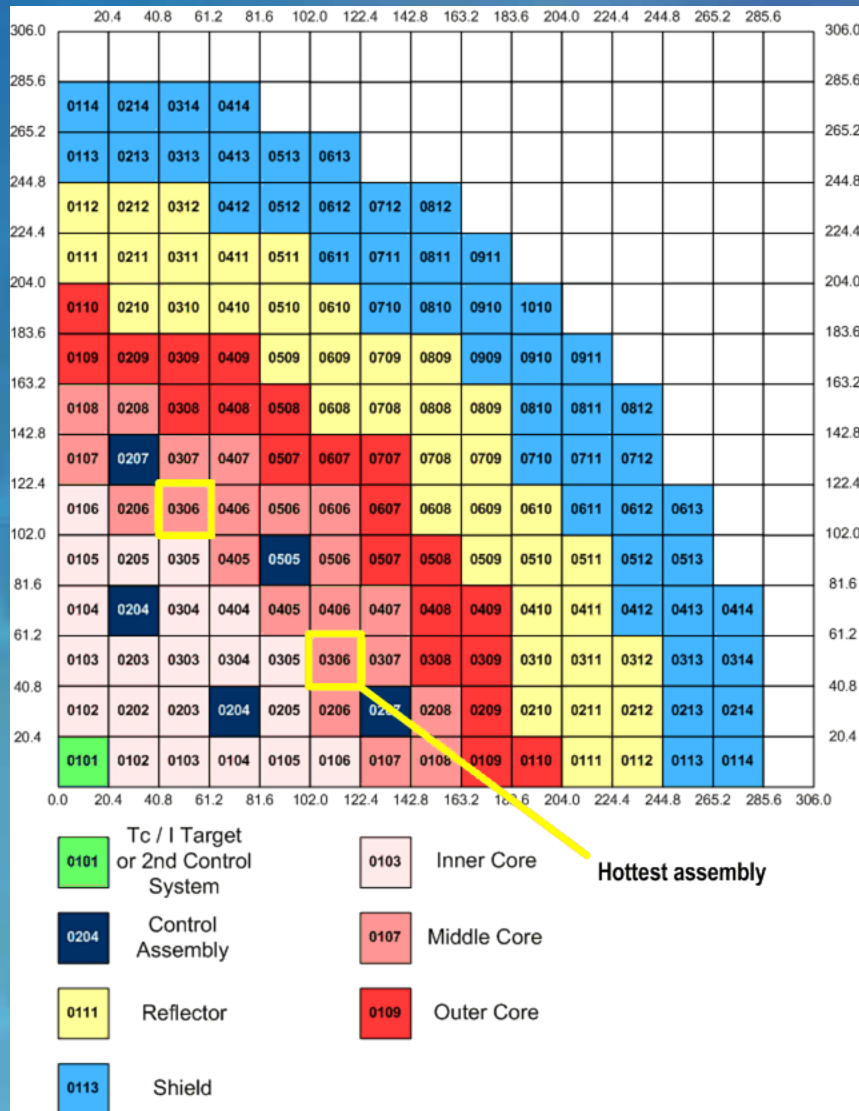


CFX Numerical Results (3x3)

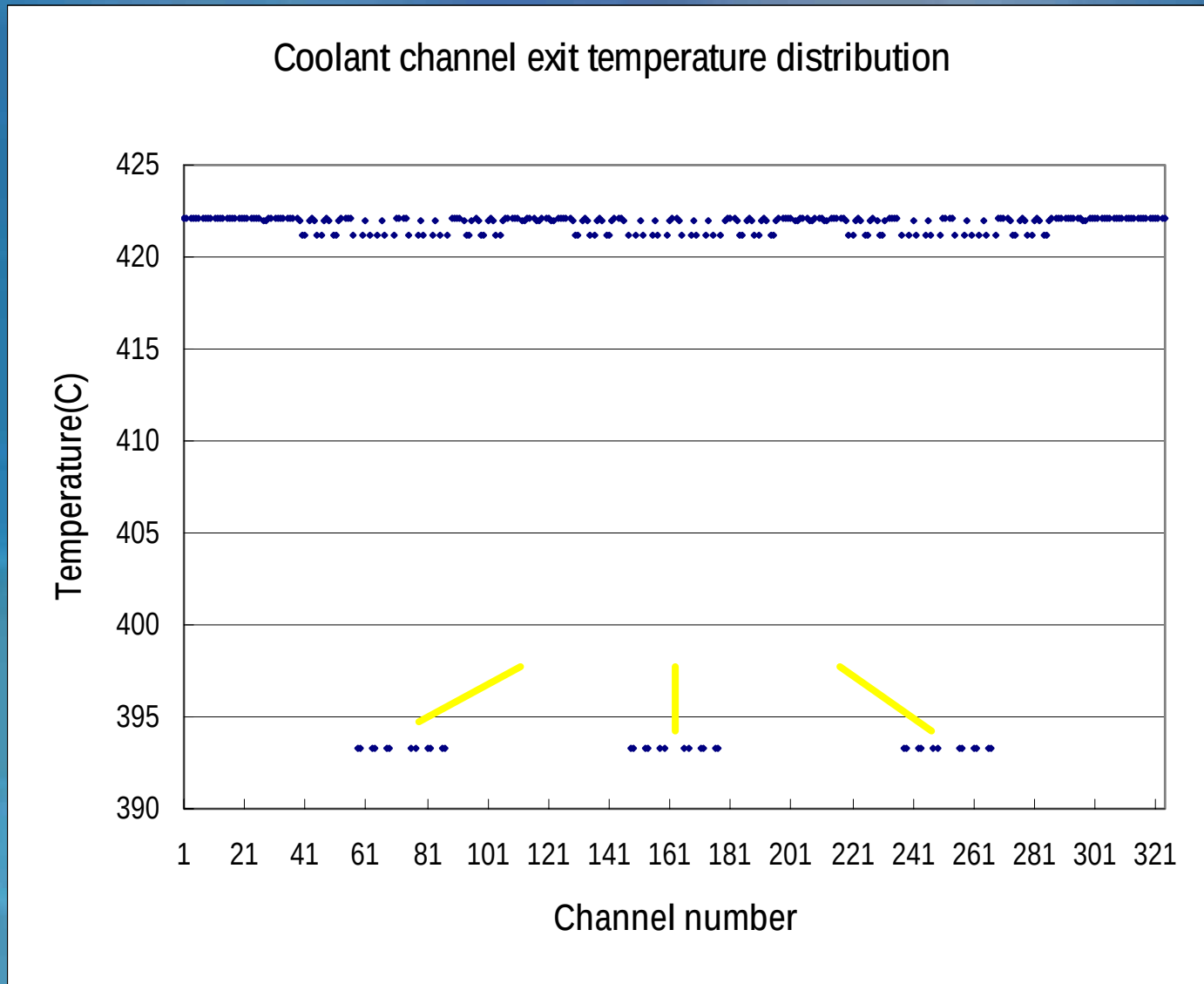
- Axial temperature distribution at center of subchannel



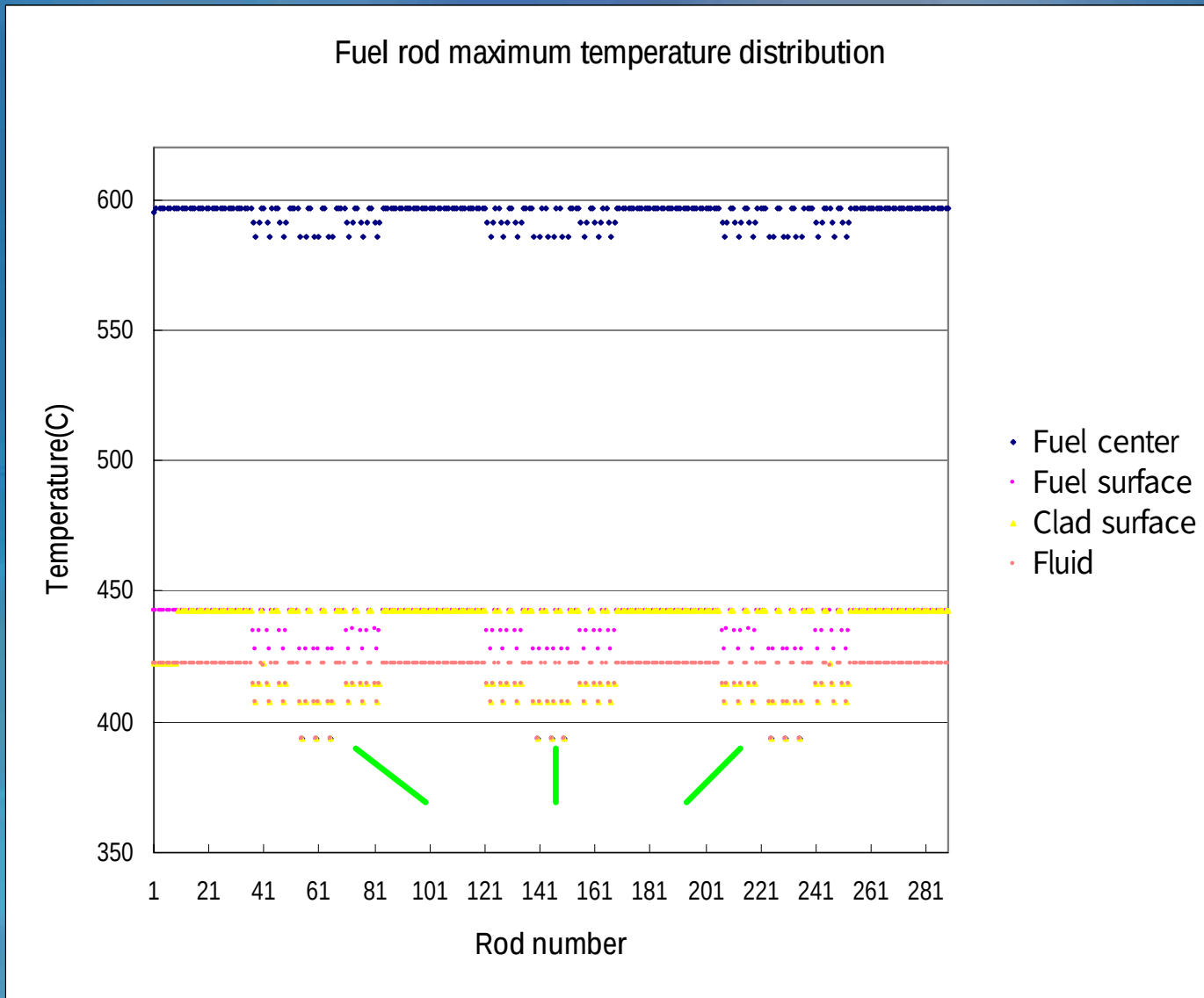
Region of Interest (17x17)



MATRA Computational Results (17x17)

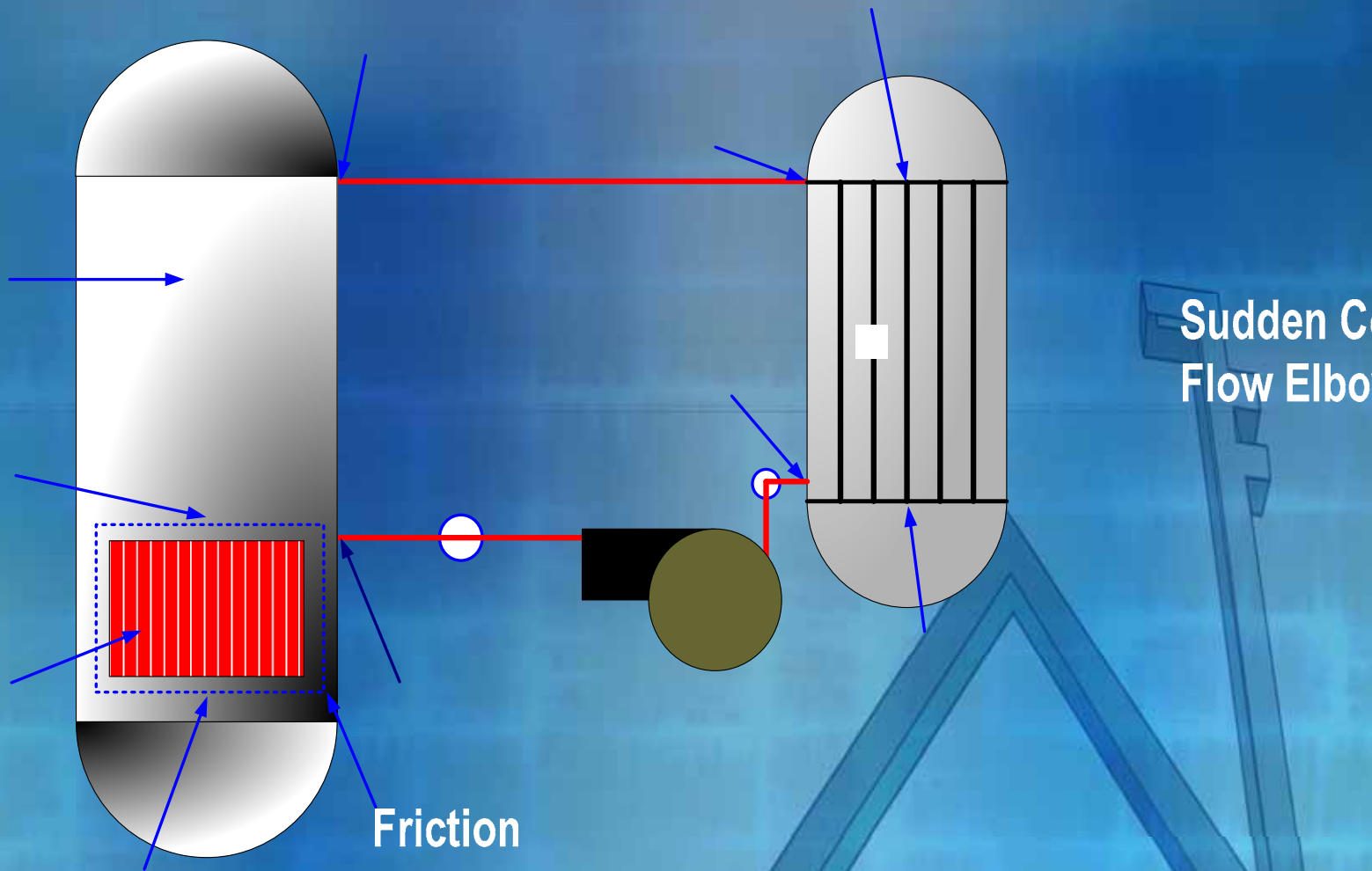


MATRA Calculation Results (17x17)

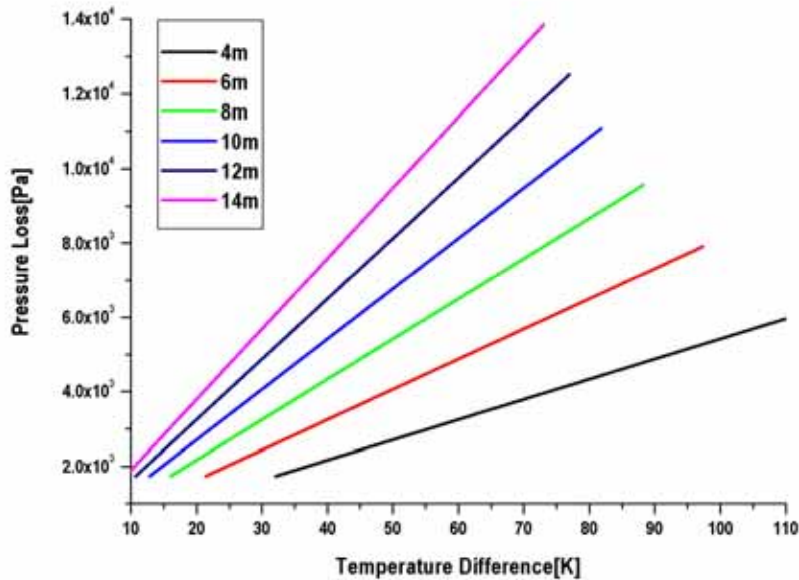


Scaling Analysis

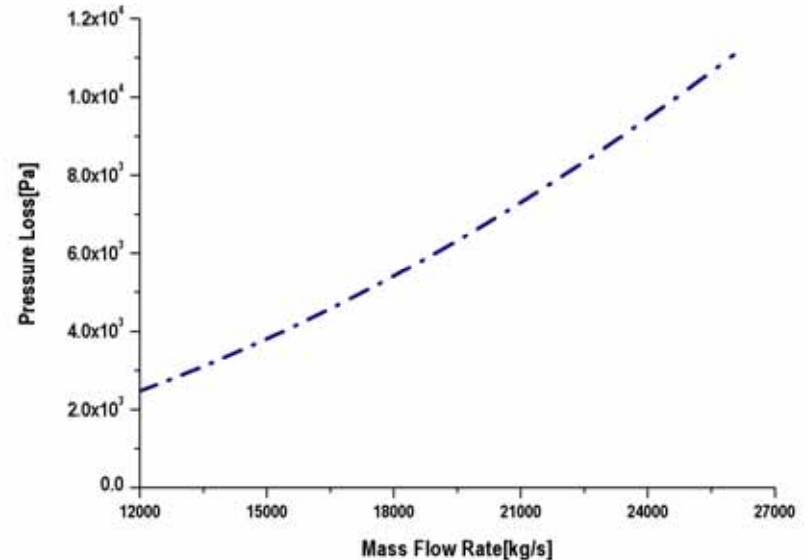
PEACER Primary System



Pressure Loss in PEACER

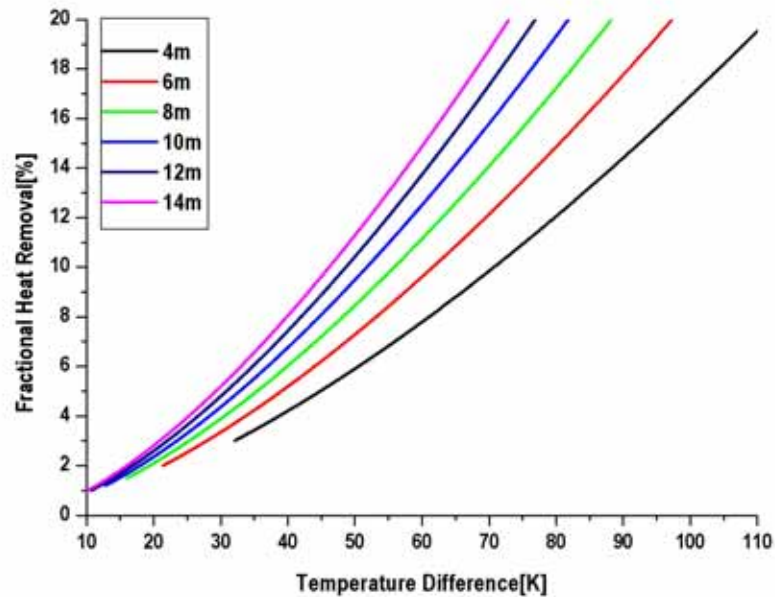


Pressure Loss According to Thermal Center Difference



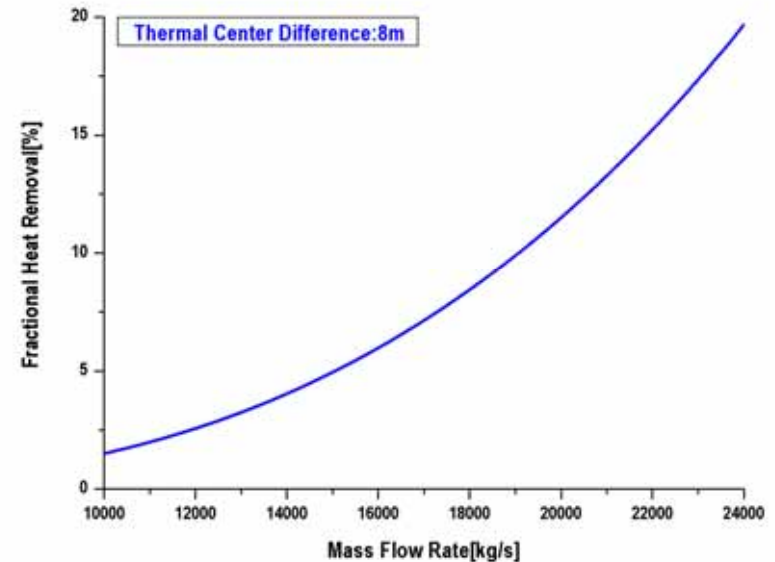
Pressure Loss According to Mass Flow Rate

Natural Circulation Capacity of PEACER



Heat Removal According to Thermal Center Difference

Heat Removal According to Mass Flow Rate



Scaling Analysis

Continuity	Momentum Equation
$U_i = \frac{a_o}{a_i} U_r$	$\rho \frac{dU_r}{dt} \sum_i \frac{a_o}{a_i} l_i = \beta g \rho \Delta T l_h - \rho \frac{U_r^2}{2} \sum_i \left(f \frac{l}{d} + K \right) \left(\frac{a_o}{a_i} \right)^2$

$$Ri = \frac{g \beta \Delta L \Delta T}{U^2}$$

$$F = \sum \left(f \frac{L}{D} + K \right)$$

Design Parameter	PEACER	HELIOS
Richardson Number	14.80	14.80
Friction Number	29.5	7.5
Thermal Center Difference [m]	8	8
Velocity in Core [m/s]	0.199	0.199
ΔT [°C]	55.4	55.4
Thermal Power	156 MW	9.3 kW



The diagram illustrates the Pb-Bi loop system, which is a closed-loop circulation system for a liquid metal coolant. The system is divided into several functional areas, each highlighted by a red box:

- Core mockup system-02:** This area contains the core mockup, which is a vertical assembly of tubes. It includes a heater at the bottom, a pressure gauge, and an Ar injection point. The core mockup is connected to a bottom tray.
- Cover gas system-03:** This system is located at the top of the core mockup. It includes an OCS (Oxygen Control System) and a vent line. It is connected to the top of the core mockup and has a level buffer for impurity control.
- HX system-04:** This is a heat exchanger system. It consists of a vertical bundle of tubes (2 tube-20 mm dia., 2 m long) with a temperature and flow sensor. It is connected to the top of the core mockup and has an Ar injection point.
- Storage system-01:** This system is located at the bottom right. It includes a storage tank, a vent line, and a flange. It is connected to the bottom of the core mockup and has a gas injection system.

The main circulation loop is shown with a central vertical pipe. The flow is driven by a Pb-Bi Pump-07. The system is designed to operate at 400 °C and 6.83 kg/s. The flow is controlled by various valves and sensors, including Orifice-05 and Impurity control-06. The system is also equipped with a bypass line and a heater for the core mockup.

HELIOS Design

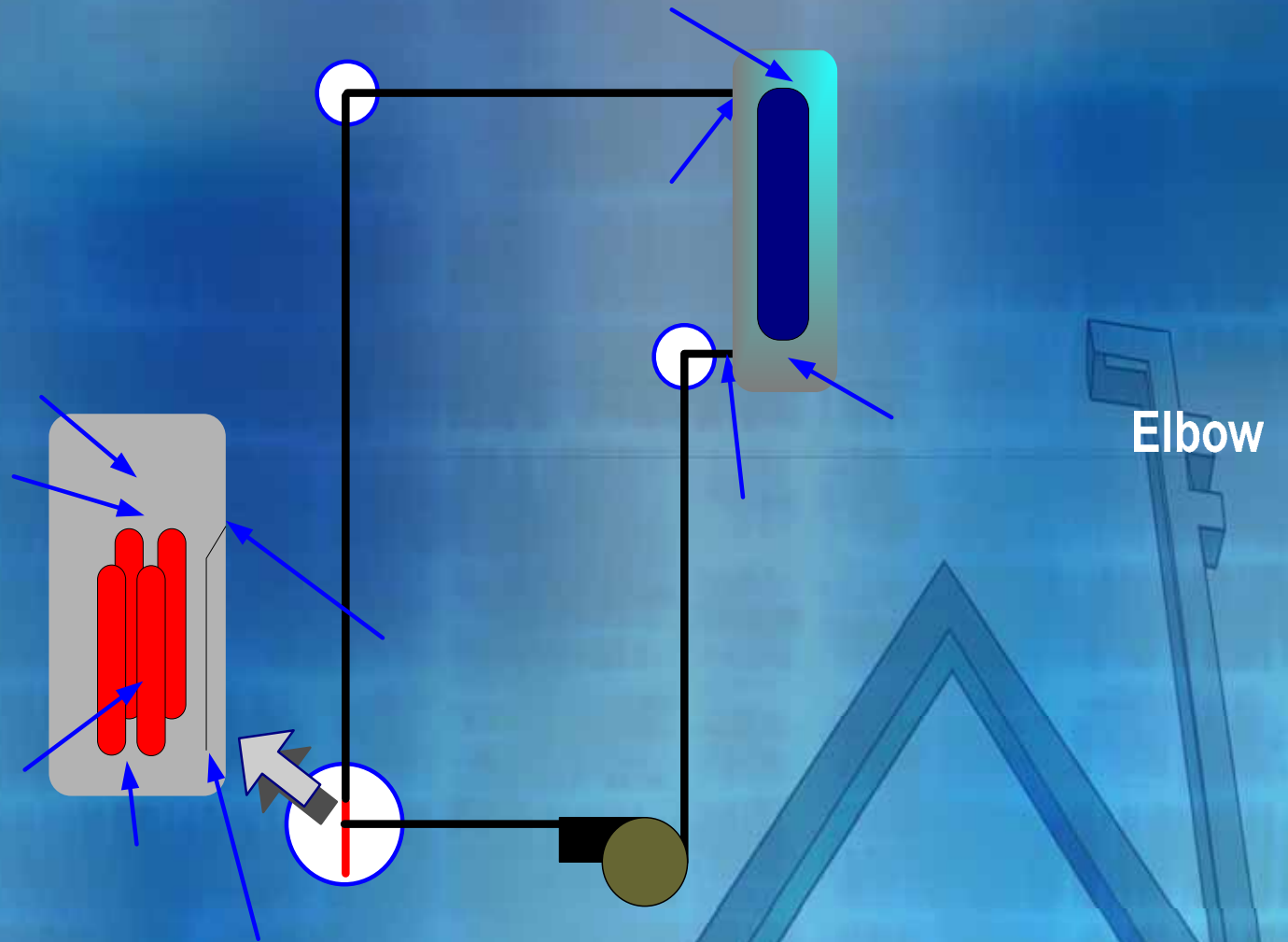
Initial Conditions

Parameter	PEACER	HELIOS
Number of Loops	2	1
Flow Area of Core [m ²]	9.4371	0.0020
Hydraulic Diameter [m]	0.01703	0.0271
Thermal Center Difference [m]	8	8

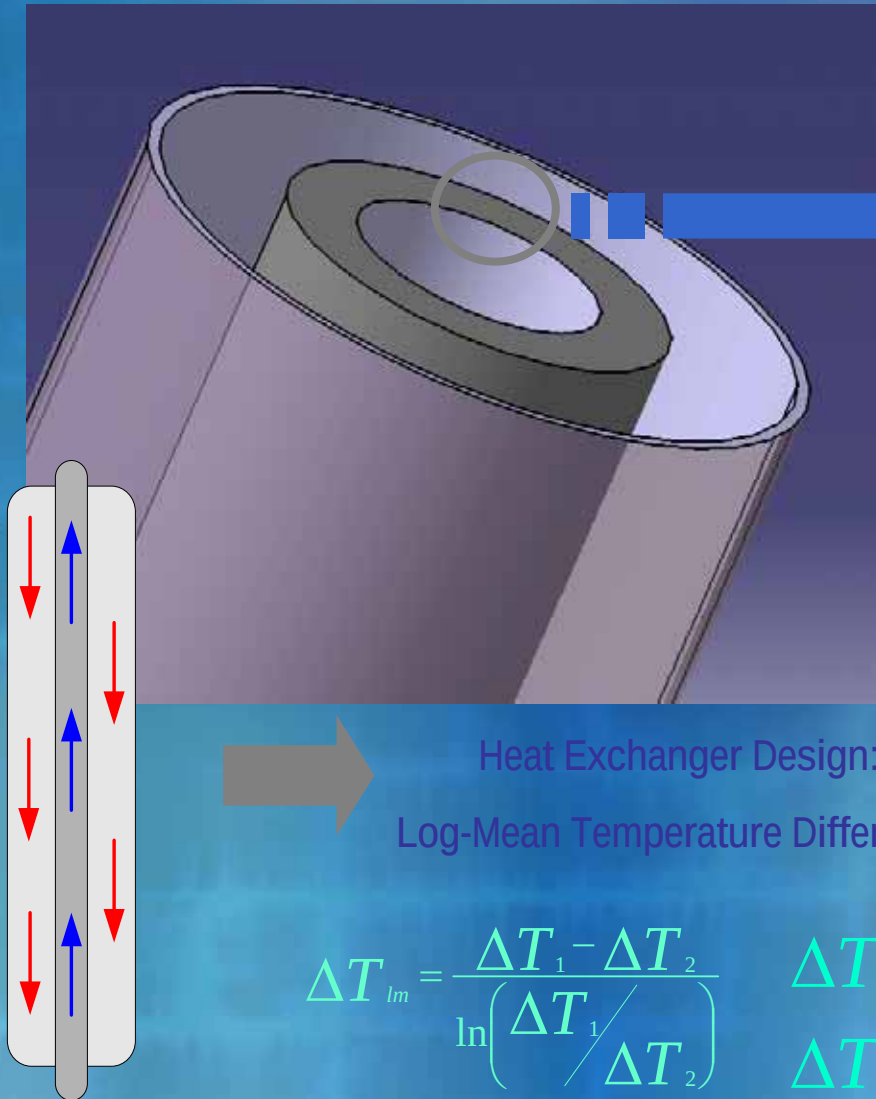
Natural Circulation Results

Parameter	Value
Decay Power [MW _{th}]	156
Mass Flow Rate [kg/s]	19,237
Temperature Difference [K]	55.4
Velocity in Core [m/s]	0.199

HELIOS Schematic Diagram



Heat Transfer Mechanism

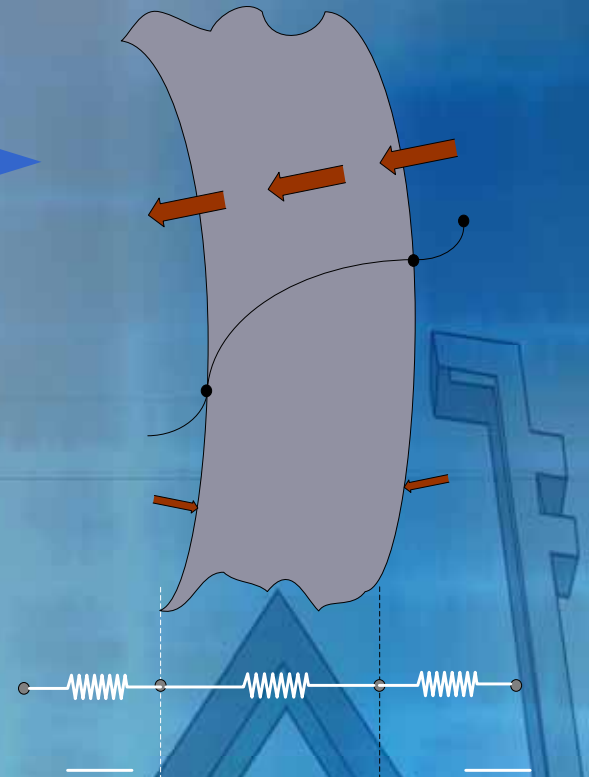


Heat Exchanger Design:
Log-Mean Temperature Difference

$$\Delta T_{lm} = \frac{\Delta T_1 - \Delta T_2}{\ln\left(\frac{\Delta T_1}{\Delta T_2}\right)}$$

$$\Delta T_1 = \Delta T_{Pb-Bi,in} - \Delta T_{W,out}$$

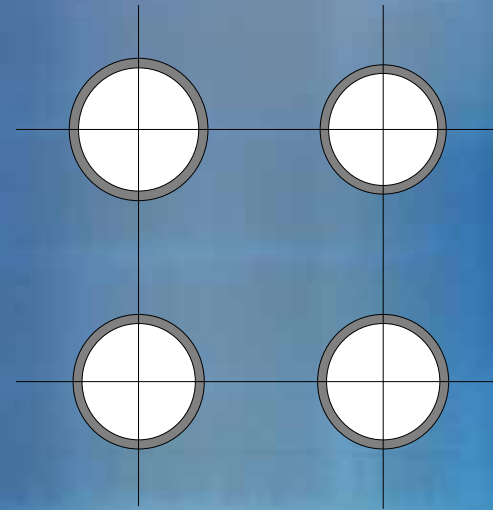
$$\Delta T_2 = \Delta T_{Pb-Bi,out} - \Delta T_{W,in}$$



Subchannel Analysis

Step 1

General Friction Factor
-Core & SG: Square Lattice

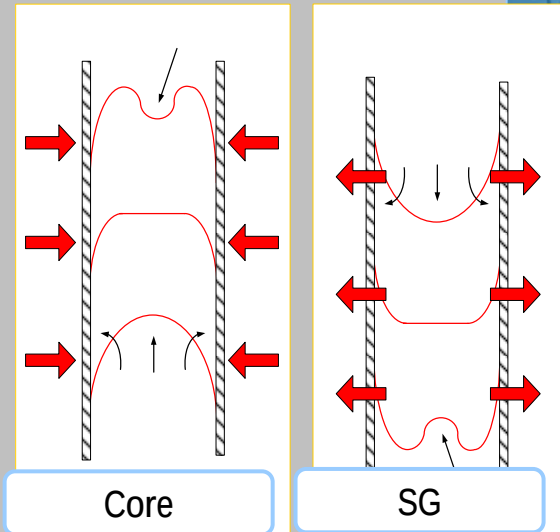


Step 2

Mixed Convective Friction Factor

Core: Square Lattice
Heated Upward Flow

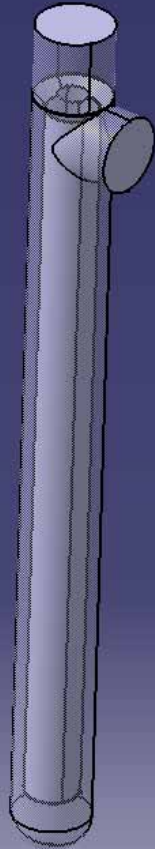
SG: Triangular Lattice
Cooled Downward Flow



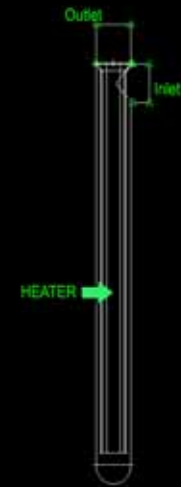
From CAD to CFX

Heating Region

CAD Modeling

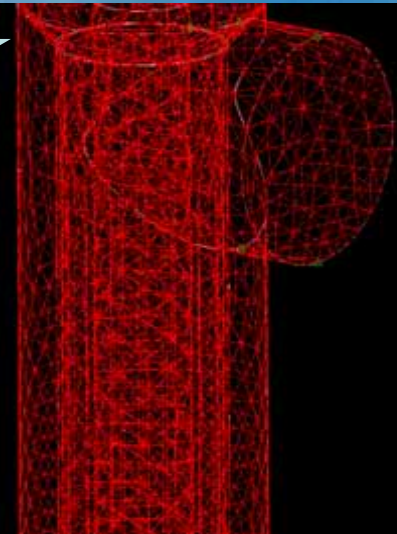


Importing



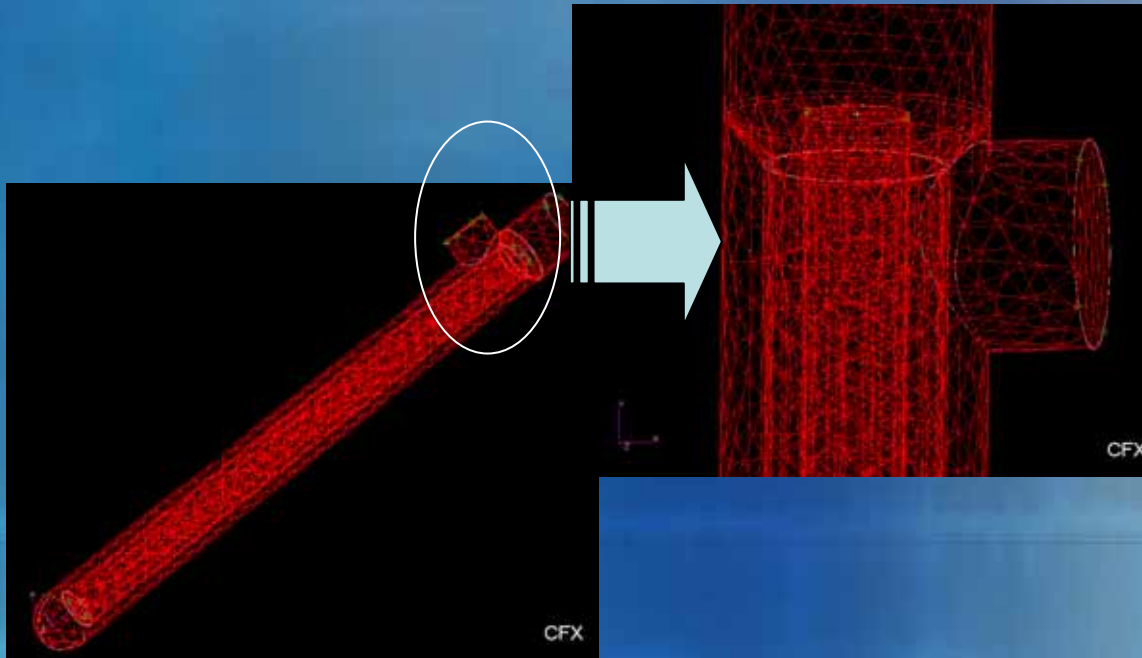
CFX

Meshing



CFX

Solver Boundary Condition



Inlet Boundary Condition

- Mass Flow Rate: 6.83 kg/s

Outlet Boundary Condition

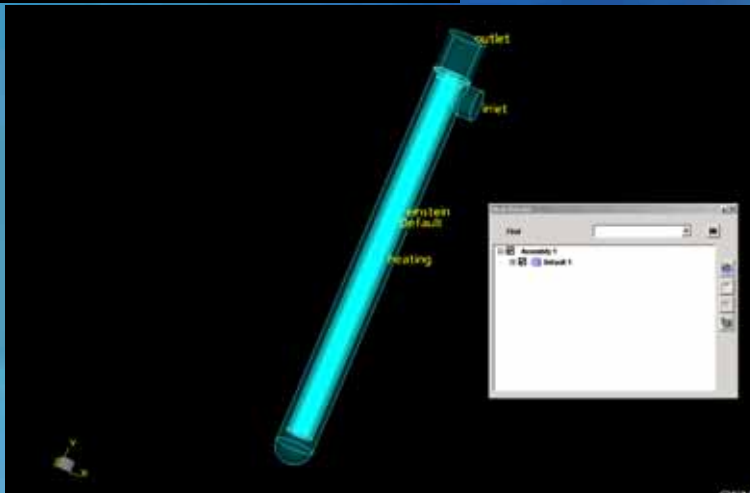
- Mass Flow Rate: 6.83 kg/s

Heating Source

- Heat Flux: 3183 kW/m²

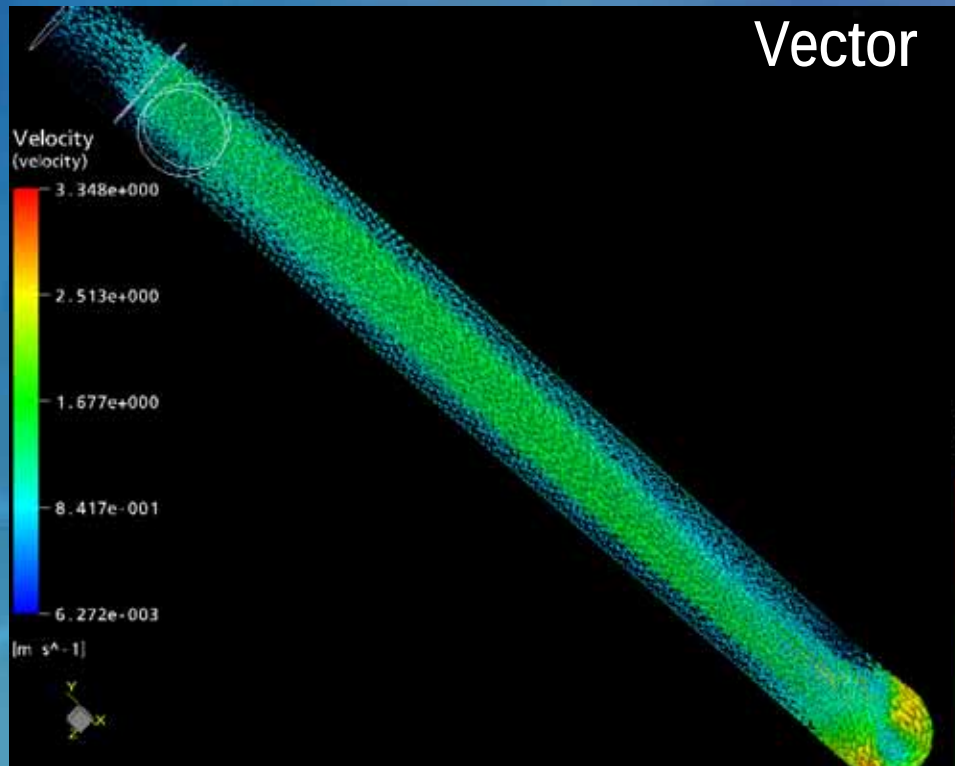
Iteration Number: 1000

Residual: 0.00001

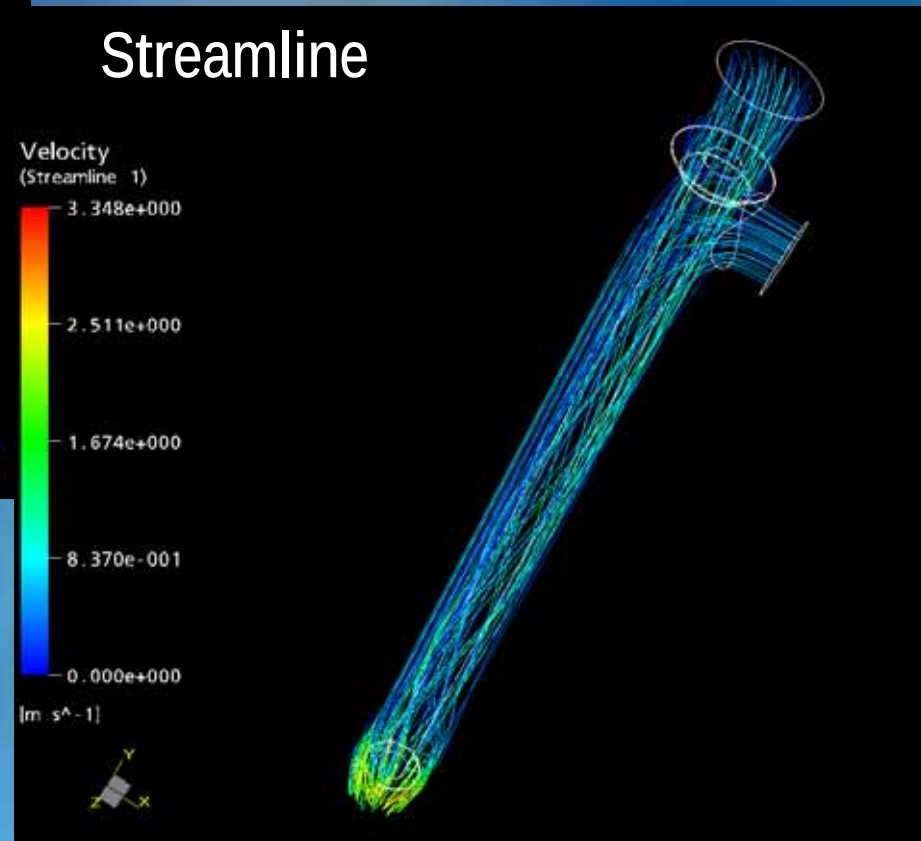


Result - Velocity

Vector



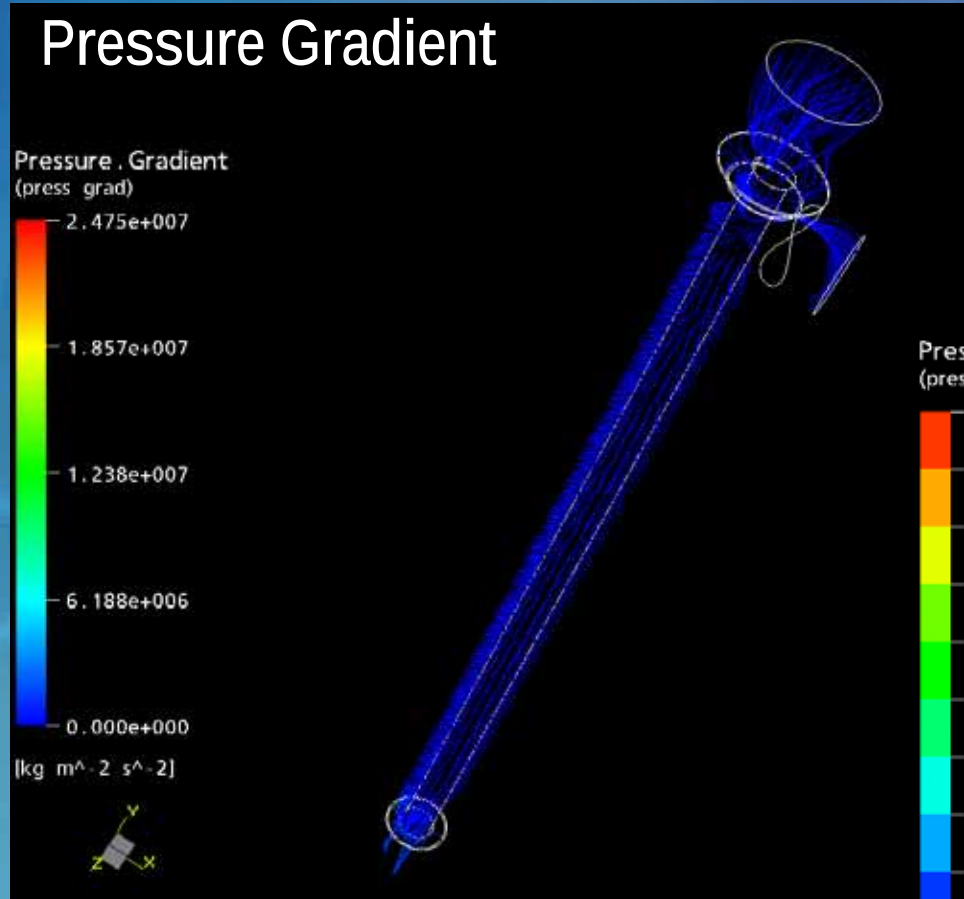
Streamline



Result - Pressure

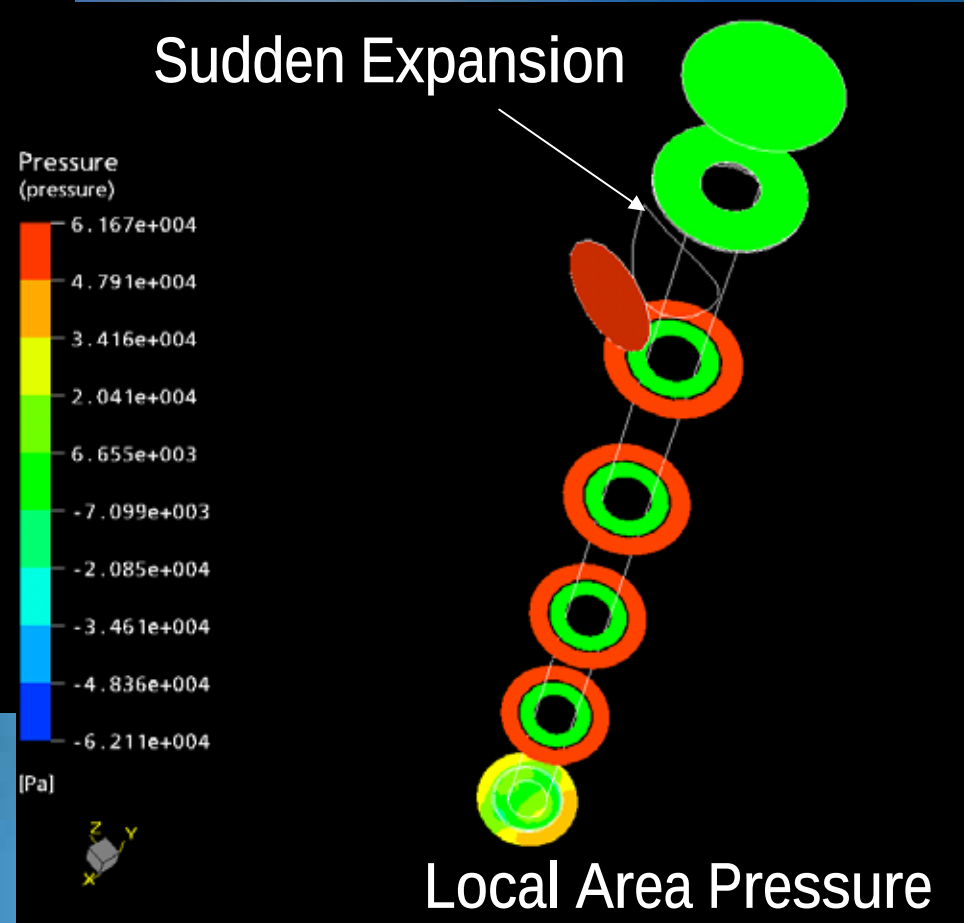
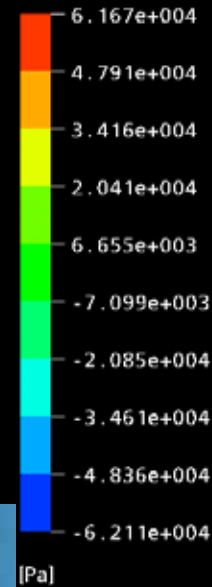
Pressure Gradient

Pressure , Gradient
(press grad)



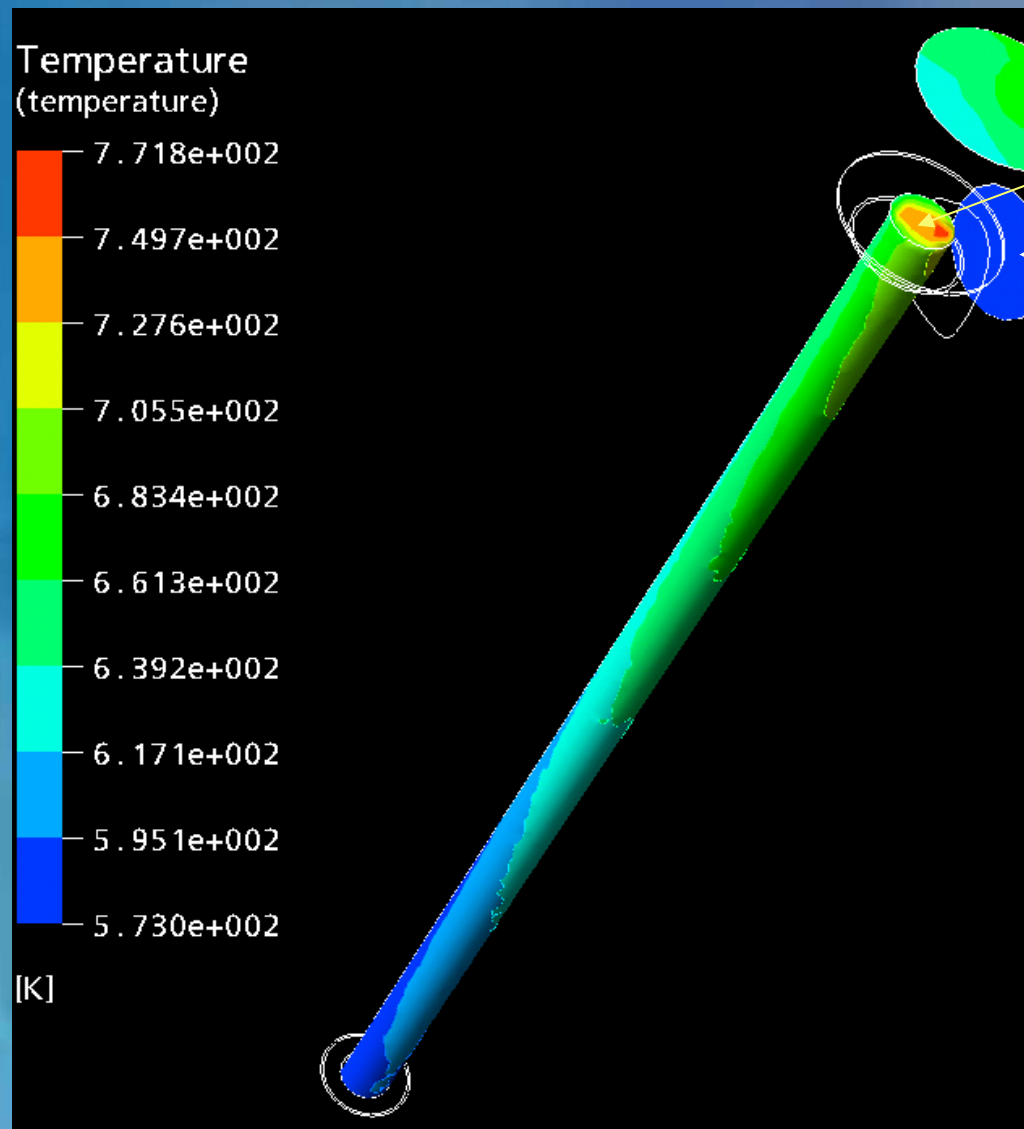
Sudden Expansion

Pressure
(pressure)



Local Area Pressure

Result - Temperature



Outlet: 400°C

Inlet: 300°C